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744 Heartland Trail 53717-1934 P.O. Box 8923 53708-8923 Madison, WI Telephone: 608-831-4444

Telephone: 608-831-4444 Fax: 608-831-3334

# PREDESIGN INVESTIGATION RESULTS LANDFILL GAS AND LEACHATE COMPONENTS

# H.O.D. LANDFILL SITE USEPA DOCKET NO. V-W-99-C-543

# VILLAGE OF ANTIOCH LAKE COUNTY, ILLINOIS

PREPARED FOR WASTE MANAGEMENT OF ILLINOIS, INC.

PREPARED BY RMT, INC.

May 2000

James M. Timijim	5/03/2000
James M. Tinjum, P.E. On-site Coordinator	Date
Bernd Rehm, P.G. Predesign Studies Task Leader	5/3/00 Date
Moch J. Tonesoni Mark J. Torresani, P.E.	5/3/2000
Mark J. Torresani, P.E.	Date
Project Manager	

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# **Section 1** Introduction

In accordance with the approved Predesign Investigation and Remedial Design/Remedial Action Workplan (RMT, 1999), Predesign Investigations (PDI) were conducted to obtain additional information necessary for initiating the Remedial Design (RD) at the H.O.D. Landfill site in Antioch, Illinois. As part of the PDI, a landfill gas (LFG) and leachate collection field investigation was conducted.

#### 1.1 Background and Scope of the Landfill Gas Investigation

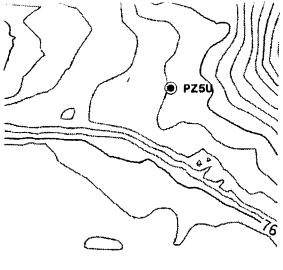
The Statement of Work (SOW) requires the installation of an active landfill gas (LFG) system at the facility, or an upgrade of the existing passive gas system, or some combination of the two. The objective of an LFG management system is to prevent off-site gas migration and to limit the build-up of LFG within the waste mass. The RD will propose to collect and treat the LFG in a controlled manner, and to control the migration of LFG.

Landfill gas sampling was performed to assess the design parameters for implementing an active gas management system and parameters to meet air permit requirements. This study was conducted to determine the viability of incorporating existing extraction points into an active gas extraction system and to identify new extraction points, if any, which may be needed to implement an active gas management system. This study will be used to evaluate the requirements of an LFG system that is sufficient to control the LFG at the site.

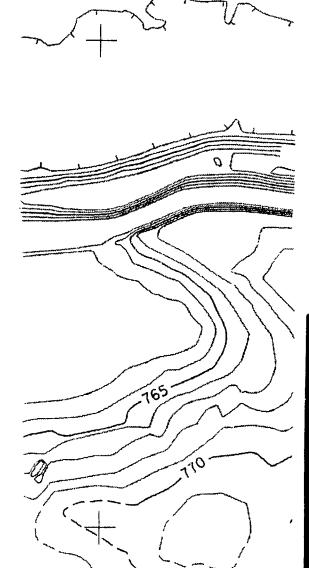
#### 1.1.1 **Physical Inspection**

The condition of the existing 14 gas well flares (GWF1 to GWF14), the existing 14 leachate piezometers (LP1 to LP14), and the leachate extraction points (P1, P2A, P3A, P8, P9, and P10) were assessed to determine if they could be utilized as part of a gas management system to be implemented during the RA. The locations of the wells that were physically inspected are shown on Figure 1. The inspections of each gas well, leachate piezometer, leachate extraction point, and final cover consisted of the following:

- Inspection of the condition of aboveground well and flare components (condition of well pipe, vertical orientation, condition of flares)
- Evaluation of well data (stick-up height, total depth, liquid depth)
- Inspection of the landfill cap for indications of gas migration, such as stressed vegetation, odors, and (if the cover is saturated) gas bubbles emanating from the cover soil.

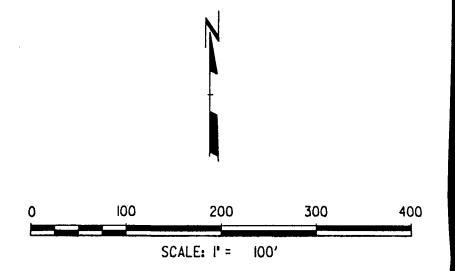


- 3. THE FACILITY BOUNDARY WAS INTERPRETED BY R.E. ALLEN AND ASSOCIATES, LTD.
- 4. VERTICAL DATUM IS REFERENCED TO NATIONAL GEODETIC VERTICAL DATUM (NGVD) OF 1929.
- 5. LEACHATE LEVELS WERE RECORDED ON NOVEMBER 8 AND 9, 1999 BY RMT, INC.
- 6. THE AVERAGE SHALLOW WATER LEVELS RECORDED FOR THE EXTERIOR MONITORING WELLS DURING THE DECEMBER, 1999, GROUNDWATER PDI ARE INDICATED IN PARENTHESIS NEXT TO THE WELLS MONITORED.



WASTE MANAGEMENT





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PROJECT: WASTE MANAGEMENT OF ILLINOIS, INC.
H.O.D. LANDFILL
PREDESIGN INVESTIGATION

#### SHEET TITLE:

### LEACHATE LEVELS FOR NOVEMBER 1999

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CHECKED BY:	JMT	I*=100′	FILE NO. LEACHATE.PLT
APPROVED BY:	MJT	DATE PRINTED:	EICUDE 4
DATE: MAY 2000		MAT U 3 ZUUU	FIGURE 1



744 Heartland Trail Madison,WI 53717-1934

P.O. Box 8923 Madison, Wi 53708-8923 Phone: 608-831-4444 The information collected was used to determine which wells and probes are suitable for incorporation into an active gas collection system, as described in Section 3 of this report.

### 1.1.2 Gas Analysis

Landfill gas is composed of two major gas constituents, methane (CH<sub>4</sub>) and carbon dioxide (CO<sub>2</sub>). These gas constituents, along with oxygen (O<sub>2</sub>) and balance gas (primarily nitrogen), were analyzed in the field during the pilot investigation using a portable gas analyzer.

### 1.2 Background and Scope of the Leachate System Investigation

The SOW requires that a pilot/predesign study be conducted to determine the viability of using the existing extraction points for the withdrawal of leachate from the site. The existing extraction points are to be considered for use in a dual landfill gas and leachate extraction system to be implemented as part of the RA. According to the SOW, the purposes of the leachate extraction system are as follows:

- 1. To increase leachate collection efficiencies
- 2. To reduce leachate levels throughout the landfill to eliminate seeps
- 3. To induce an inward gradient to control and collect shallow groundwater in the surficial sand aquifer in the vicinity of the site

A WMII pumping test conducted at MHE prior to the RI indicated that leachate pumping rates of 30 gpm to 40 gpm could not be sustained for extended periods once liquid volumes contained in the system storage (i.e., manhole, lateral piping, gravel bedding) had been removed. After removing the leachate from storage, the manhole went dry and recharged at a slow rate.

Based on information from the RI (Montgomery Watson, 1997), the leachate piezometers were constructed using a washed pea gravel filter pack around 6-inch-inner-diameter (ID) Schedule 80 PVC 0.020-inch slotted screen, with hydrated bentonite filling the annular space above the filter pack around the 6-inch PVC riser pipe (Montgomery Watson, 1997). Locking protective casings were installed over the riser pipes. The wells were screened from approximately 0 to 5 feet above the base of the landfill to approximately 0.5 to 4.6 feet below the base of the landfill cap. This construction method was chosen so that the wells could be used for extraction of leachate and landfill gas from the site.

This field investigation was performed to assess the condition of the existing leachate collection system in place at the site and to assess the viability of using extraction points for the

withdrawal of leachate from the site. This investigation also provides data necessary for the design of an automated system to further reduce leachate levels throughout the landfill and establish an inward gradient condition within the site. In Section 3 of this report, the viability of using existing extraction points is assessed, and any new extraction points needed to develop such a system are identified. The viability of operating this system in conjunction with the LFG collection and treatment system is also evaluated in this report.

The field investigation of the existing leachate extraction system was similar to the investigation of the LFG system with the following additions:

- Inspection of the condition of the existing leachate extraction equipment, including pumps, gauges, electrical lines, supporting pipelines, manholes, and collection lines.
- Inspection of the downhole condition. A section of PVC pipe (equivalently sized to leachate pumps expected to be utilized for the RA) was lowered to check for kinks, well casing breaks, or other obstructions that would render the well unusable for gas extraction.

Information collected during the inspection of existing extraction points and the existing leachate collection system is utilized to determine which components are suitable for incorporation into an automated leachate extraction system to be implemented as part of the RA.

# Section 2 Landfill Gas Investigation

### 2.1 Physical Evaluation of Existing Well Locations

### 2.1.1 Condition of Aboveground Well and Flare Components

Prior to the field PDI, the aboveground portions of the 14 gas well flares were dismantled by WMII to allow for collection of well data by RMT field personnel. Dismantling was achieved either by removing the flare component at the flange connecting the PVC riser to the flare stem, or by cutting the PVC riser near the flange. The vertical orientation of the flares was not fully assessed (i.e., only the PVC riser could be observed for vertical orientation). The gas well PVC risers were temporarily sealed following removal of the flare units.

Observation of the condition of the flares was conducted as these components were lying on the ground in proximity to the well locations. The gas well flares were generally in poor condition with the flare stems slightly rusted/corroded and the wind screens heavily rusted/anodized and often cracked.

The PVC riser pipe was generally in good condition. Often, the pipe was stained orangish/red. This was most likely rust staining from the steel flare units mounted on the PVC risers. The PVC risers for GWF 1 through GWF 14 were generally near vertical, with the exception of GWF 6, which was tilted approximately 10 degrees. Full descriptions of the gas well flare's condition are contained in the field notebook (Appendix A). In addition, photographs of representative well locations are contained in Appendix B.

#### 2.1.2 Well Data

Field measurements were made of the 14 existing gas well flares (GWF 1–14), the existing 14 leachate piezometers (LP1-14), and the leachate extraction points (P1, P2A, P3A, P8, P9, and P10), including stick-up height, total depth, and liquid depth. This information is given in Tables 1 and 2. Full details on the construction of these wells (including the as-constructed screen interval) are included in Appendix C of this report.

Table 1 Landfill Gas and Leachate Measurements in the New<sup>(1)</sup> Landfill H.O.D. Landfill

LOCATION	% CH₄	% O <sub>2</sub>	% CO <sub>2</sub>	% BALANCE GAS	CALCULATED % LEL <sup>(2)</sup>	GROUND SURFACE EL <sup>(3)</sup> (ft A.M.S.L.)	MEASURED STICKUP <sup>(4)</sup> (ft)	WELL DEPTH (ft BGS) <sup>(5)</sup>	MEASURED BOTTOM OF WELL EL (ft A.M.S.L.)	LEACHATE LEVEL (ft BGS) <sup>(5)</sup>	APPROXIMATE LEACHATE EL (ft A.M.S.L.)	WELL DIAMETER (in)
GWF1	64	0.1	32.7	3.1	100+	795.1	1.5	40.5	754.6	31.9	763.2	8
GWF2	64	0.3	32.9	3	100+	795.5	1.6	46.4	749.1	29.2	766.3	8
GWF3	62.5	0.2	32.9	4.1	100+	794.1	3.0	41.0	753.1	36.1	758.0	8
GWF4	63.5	0.2	36.2	0.1	100+	791.5	2.6	43.4	748.1	37.5	754.0	8
GWF5	45.2	6.1	26.2	22.4	100+	785.3	3.3	42.7	742.6	22.8	762.5	8
GWF6	66.2	0.2	33	0.7	100+	785.8	3.5	37.5	748.3	15.8	770.0	8
GWF7	64.5	1.3	29.5	3.5	100+	795.0	3.8	44.2	750.8	26.9	768.1	8
GWF8	16.8	15.4	9.4	58.4	100+	795.0	1.5	43.5	751.5	17.0	778.0	8
GWF9	62.5	0.6	33.4	3.5	100+	794.0	2.4	44.6	749.4	31.3	762.7	8
GWF10	64	0.1	33.5	2.5	100+	792.4	1.3	40.7	751.7	25.8	766.6	8
GWF11	69	1.6	21	8.8	100+	790.5	2.9	29.1	761.4	5.8	784.7	8
GWF12	0	20.9	0.2	78.9	0	790.9	2.1	15.9	775.0	5.0	785.9	8
GWF13	62.7	0	37.3	0	100+	791.3	3.5	41.5	749.8	21.4	769.9	8
GWF14	61.8	0.1	38.1	0	100+	790.5	2.4	36.6	753.9	22.3	768.2	8
LP5	62.9	0.4	33.8	2.9	100+	796.8	3.5	49.5	747.3	33.5	763.3	6
LP6	0.4	21	0.2	78.5	8	793.4	3.5	34.5	758.9	8.4	785.0	6
LP7	65.4	0	34.7	0	100+	791.5	4.3	51.7	739.8	11.2	780.3	6
LP8	62.5	0	37.5	0	100+	790.5	3.7	61.3	729.2	28.5	762.0	6
LP9	63.6	0	36.4	0_	100+	796.2	2.9	64.1	732.1	18.5	777.7	6
MHE	NM	NM	NM	NM	NM	791.0	2.0	36.0	755.0	21.6	769.4	30
P1	63.5	0.1	32.5	3.9	100+	792.0	3.3	NM <sup>(6)</sup>	NM <sup>(6)</sup>	25.4	766.7	6
P2A	65	0	35	0	100+	793.6	3.2	71.8	721.8	52.1	<b>74</b> 1.5	3.75
P3A	63	0.1	36.9	0	100+	786.5	3.9	61.1	725.4	27.3	759.2	3.75
P8_	62.5	0	37.5	0	100+	787.5	3.5	NM <sup>(6)</sup>	NM <sup>(6)</sup>	20.4	767.1	4
P9	0.4	20.6	0.3	78.7	8	785.3	6.1	35.9	749.4	7.3	778.0	4
P10	6.9	19.1	3.1	71.2	100+	785.1	3.6	NM <sup>(6)</sup>	NM <sup>(6)</sup>	23.4	761.7	4

Last updated: 4/25/00 By: JMT QC: MJT

Notes:

(1) The "new" landfill comprises 26.8 acres located immediately east of the "old" landfill.
(2) Lower explosive limit, with 5 percent methane equivalent to 100 percent LEL.
(3) Elevation interpolated from March 4, 1999, aerial photography.
(4) Field measured, ground surface to top of PVC casing.
(5) Feet below ground surface.
(6) Existing leachate extraction equipment created an obstruction to lowering the PVC probe.

Table 2 Landfill Gas and Leachate Measurements in the Old<sup>(1)</sup> Landfill H.O.D. Landfill

LOCATION	% CH₄	% O <sub>2</sub>	% CO <sub>2</sub>	% BALANCE GAS	CALCULATED % LEL <sup>(2)</sup>	GROUND SURFACE EL <sup>(3)</sup> (ft A.M.S.L.)	MEASURED STICKUP <sup>(4)</sup> (ft)	WELL DEPTH (ft BGS) <sup>(5)</sup>	MEASURED BOTTOM OF WELL EL (ft A.M.S.L.)	LEACHATE LEVEL (ft BGS) <sup>(5)</sup>	APPROXIMATE LEACHATE EL (ft A.M.S.L.)	WELL DIAMETER (in)
LP1	3.5	20.2	1.6	75.2	70	776.3	3.0	19.0	757.3	8.3	768.0	6
LP2	66.5	0.4	27.8	4.4	100+	785.9	2.5	33.5	752.4	16.9	769.0	6
LP3	14.4	17.4	3.7	65.7	100+	778.6	3.0	25.0	753.6	12.5	766.1	6
LP4	67.2	0.3	27.5	5	100+	788.7	2.3	36.7	752.0	16.1	772.6	6
LP10	66.6	0.4	25.6	6	100+	781.2	2.9	23.1	758.1	11.2	770.0	6
LP11	65.2	0.2	30.2	4.4	100+	787.7	3.1	27.9	759.8	15.7	772.0	6
LP12	69.5	0.2	24.7	4.6	100+	782.8	5.7	19.3	763.5	14.4	768.4	6
LP13	36.5	11.8	12.5	39.8	100+	779.5	2.8	15.3	764.3	13.1	766.5	6
LP14	69.7	0	26.1	4.2	100+	782.1	2.8	21.2	760.9	16.7	765.4	6
MHW	NM	NM	NM	NM	NM	791.3	2.0	32.0	759.3	24.5	766.8	30

(1) The "old" landfill comprises 24.2 acres of the western third of the site.
(2) Lower explosive limit with 5 percent methane equivalent to 100 percent LEL.
(3) Elevation interpolated from March 4, 1999, aerial photography.
(4) Field measured, ground surface to top of PVC casing.
(5) Feet below ground surface.

Last Updated: 4/25/00

By: JMT QC: MJT

#### 2.1.3 **Downhole Condition**

A 4-inch-diameter, 4-foot-long section of PVC pipe was lowered to the full depth of each well in order to record obstructions and the amount of silt accumulation at the base of the wells. No obstructions were observed for any wells on the site. Total depth recordings are given in Tables 1 and 2. Minor silt accumulations (i.e., typically less than 6 inches) were observed when the PVC pipe probe was brought to the surface.

#### 2.1.4 **Examination of Landfill Cap**

The landfill cap was examined for any signs of gas migration, such as stressed vegetation, odors, and (if the cover was saturated) gas bubbles emanating from the cover soil. The cover vegetation was observed to be in excellent condition, with the exception of several depressed, ponded areas in the new landfill area. Specifically, the cover around GWF 6 was saturated. Some surficial soil cracking was observed at the base of several wells in the new landfill, possibly due to settlement of the landfill mass around the well. Some stressed vegetation was observed near GWF 4. No seeps were observed on any of the sideslopes. Additionally, the cover was not observed to be saturated, with the exception of the area around GWF 6. Gas bubbles emanating from the saturated area around GWF 6 were not observed.

#### 2.2 Gas Analysis

A Landtec GEM-500 portable gas analyzer was used to monitor for major gas constituents at each well location. As there were no sampling ports for any of the wells, measurements were accomplished by lowering tygon tubing approximately 2 feet into the well casing. The output of the gas analyzer is reported in percent by volume as shown in Tables 1 and 2. The GEM-500 was calibrated daily according to procedures outlined in the operations manual (Attachment D to the Field Sampling and Analysis Plan).

Landfill gas pressures could not be recorded during the field data collection. This was due to the fact that all wells were not adequately sealed from atmospheric pressure (i.e., there were no isolation valves or gas sampling ports). However, visual observations were recorded in the field notebook (Appendix A) indicating that a positive pressure build-up condition existed at a number of the gas well flares.

### 2.3 Evaluation of Landfill Gas Migration Potential

### 2.3.1 Southern Boundary

A series of wetlands traverse the southern site boundary, which reduce and/or eliminate the gas migration potential in this direction. In addition, Sequoit Creek runs along the southern site boundary. Landfill gas cannot readily migrate horizontally through saturated soil or standing water; therefore, the potential for migration to the south is considered to be very low. The exception is in the southeastern corner of the landfill where a thin unsaturated soil zone is present. For the southern boundary, geologic Cross Section A-A' of the RI (Appendix D) demonstrates that shallow water surface is at, or very close to, the surface. In addition, the incorporation of an active gas management system into the RD/RA will reduce the potential risk of landfill gas migration in this area.

#### 2.3.2 Western Boundary

Again, Sequoit Creek forms the western site boundary. Per the RI, Sequoit Creek is hydraulically connected to the surficial sand unit. The shallow groundwater system in this portion of the site either discharges to, or receives flow from, the creek, dependent on the time of the year. Similar to the southern boundary, landfill gas cannot migrate horizontally through saturated soil or standing water; therefore, the potential for migration to the west is considered to be very low. An active gas management system will be included in the RD/RA to reduce the risk of landfill gas migration in these areas.

#### 2.3.3 Eastern and Northern Boundaries

A thin (i.e., typically less than 10-foot-thick), unsaturated soil (composed of fine-grained material) zone is present outside the eastern and northern landfill perimeter. An active gas management system will be included in the RD/RA to reduce the risk of landfill gas migration in these areas.

## Section 3

# **Leachate System Evaluation**

### 3.1 Condition of Above-grade Wells and Extraction Points

As noted in the PDI field notebook (Appendix A), the PVC riser pipes for the gas well flares, leachate probes, and extraction points were generally in good condition. However, due to settlement of the waste mass relative to the well assemblage, the top of the steel protective casings often were below the top of the PVC riser pipes.

#### 3.2 Well Data

Field measurements were made of the 14 existing leachate probes (LP 1 through LP 14) and the extraction points (P1, P2A, P3A, P8, P9, and P10), including stick-up height, total depth, and liquid depth. This information is given in Tables 1 and 2 along with data on the as-constructed screen interval. Full details on the construction of these wells is included as Appendix C.

#### 3.3 Downhole Condition

A 4-inch-diameter, 4-foot-long section of PVC pipe was lowered to the full depth of each well in order to record obstructions and the amount of silt accumulation at the base of the wells. The total well depths were not measured for P1, P8, and P10 because the existing leachate extraction equipment created an obstruction to lowering of the PVC probe. Otherwise, no obstructions were observed for the remaining wells on the site. Total depth recordings are given in Tables 1 and 2. Again (as noted in the landfill gas section), very little (if any) silt accumulation was observed when the PVC pipe probe was brought to the surface.

## 3.4 Existing Leachate Extraction Components

Supporting equipment for the two existing leachate extraction manholes (MHE and MHW) was in operation during this PDI field investigation. Leachate extracted from these manholes equipped with leachate pumps is routed to, and stored in, a dedicated tanker truck for subsequent removal from the site.

The supplemental leachate extraction system (consisting of extraction points P1, P2A, P3A, P8, P9, and P10, and an above-grade transfer system), was not in operation during this PDI field investigation. With the exception of P1, the well diameters of the supplemental leachate extraction points were 4 inches or less (see Table 1). Corrugated steel manholes encased extraction points P1, P8, P9, and P10. The transfer system typically consisted of a 1 1/4-inch

leachate transfer line, a 1/2-inch compressed air line, and a heat tracer (Raychem Chemflex autotrace parallel self regulating). The leachate lines were encased with insulation.

#### 3.5 Static Leachate Volume

A calculation was completed to estimate the current volume of extractable leachate in the landfill based on leachate levels measured during this investigation and a lower leachate level of 761 feet above mean sea level (A.M.S.L.). Based on this calculation set (Appendix E), a static volume of 16.3 million gallons is expected to be extracted to lower landfill leachate levels.

To maintain an approximate lower leachate level of 761 feet A.M.S.L., continued extraction would be required to account for infiltration, inflow from the surrounding aquifer, recovery of perched leachate, and continued waste consolidation.

# **Section 4 Summary of Key Findings** and Conclusions

#### Landfill Gas 4.1

- The presence of surface water bodies and wetlands bordering the site (e.g., Sequoit Creek) limit the potential for gas to migrate off-site along the site's western and southern perimeter. An unsaturated soil zone is present along portions of the eastern and northern landfill perimeter. The potential for this unsaturated zone to allow a pathway for horizontal LFG migration should be evaluated during the RD phase.
- Existing leachate probes (LP 1 through LP 14) and leachate extraction points (P1, P2A, P3A, P8, P9, and P10) are suitable for conversion to an active LFG extraction system because (1) well screens are situated throughout the waste mass with sufficient top cover, (2) well construction details indicate that the well pack and surface seals were adequately constructed for this conversion, and (3) physical inspection indicates that the wells are in good condition.
- For the above reasons, existing gas well flares (GWF 1 through GWF 14) are also suitable for continued use as LFG extraction wells with retrofits at the surface to account for differential settlement experienced and expected regrading and cover placement.

#### 4.2 Leachate Collection System

- Existing leachate probes (LP 1 through LP 11, and LP 14), gas well flares (GWF 1 through GWF 10, GWF 13, and GWF 14), and leachate extraction points are suitable for incorporation into an active leachate extraction system because (1) the base of the well screens are below elevation 761.7 feet A.M.S.L., which is the approximate average low shallow water level based on water level readings taken during the dry years of 1992, 1994, and 1995 (RMT, 2000); (2) physical inspection indicates that the wells are in good condition; and (3) the well diameters are large enough to lower typical extraction pumps to the base of the well with no obstructions noted during the PDI field investigation. The elevation of the shallow groundwater level will be confirmed in the groundwater PDI report.
- Locations LP 12, LP 13, and GWF 12 may not be suitable for incorporation into the active system because the measured total depths were 763.5, 764.2, and 775.0 feet A.M.S.L., respectively.
- Leachate extraction points P2A, P3A, P8, P9, and P10 are not suitable for incorporation into the proposed leachate management system because the small-diameter of the well casings (i.e., less than 4 inches) would prevent the installation of the proposed leachate extraction pumps.

- The existing extraction pump appurtenances, leachate transfer piping, and leachate storage facilities are not appropriate for incorporation into a long-term collection system; therefore, reuse should not be considered.
- The two existing leachate extraction manholes (MHE and MHW) can be incorporated into the final leachate collection system, with some retrofit being necessary to account for the shifting of the stacked manhole section units.

# Section 5 References

- Montgomery Watson. 1997. Remedial investigation/feasibility study. H.O.D. Landfill, Antioch, Illinois. January 1997.
- Montgomery Watson. 1998. Draft feasibility study. H.O.D. Landfill, Antioch, Illinois. February 1998.
- RMT, Inc. 1999. Predesign investigation and remedial design/remedial action workplan. H.O.D. Landfill site, Antioch, Illinois. September 1999.
- RMT, Inc. 2000. Prefinal remedial design report. H.O.D. Landfill site, Antioch, Illinois. April 2000.

# Appendix A Field Notebook



PROJECT NAME:	H.O.D. LANDFILL ENGINEERING PREDESIGN INVESTIGATION
PROJECT NUMBER:	5314.04
LOCATION:	ANTIOCH, ILLINOIS
DATES OF FIELD WORK:	NOVEMBER 8-9,1999
	PREDESIGN STUDY TO DETERMINE THE VIABILITY OF USING EXISTING EXTRACTION POINTS AS PART OF A DUAL EXTRACTION SYSTEM
WORK PERFORMED BY:	JAMES TINJUM MARK TORRESANI ("108/97 A.M)

Figned Date Date

Mach J. Torresons 1/5/2000 QC'd By Date



#### **GENERAL NOTES**

PROJECT NAME: HOD LANDFILL	DATE: 11 08 99
PROJECT NUMBER: 5314.04	AUTHOR: JAMES TINJUM
TIME ARRIVED ON-SITE: 9:15	TIME LEFT SITE: \8:00

WEATHER: SUNNY, FORECAST HIGH NEAR 70° F

#### WORK/SAMPLING PERFORMED:

GAS, LEACHATE DEPTH, AND WELL DEPTH
MEASUREMENTS AT THE FOLLOWING LOCATIONS:
LPI, LPZ, LP3, LP4, LP10, LP11, LP12, LP13, LP14, GWF1, LP5,
GWF9, GWF10, LP6, GWF11, P10, GWF2, P1, GWF3
PROBLEMS ENCOUNTERED/CORRECTIVE ACTIONS TAKEN:

DID NOT DETERMINE TOTAL DEPTHS AT PI AND PID DUE TO EXISTING PUMPING EQUIPMENT IN WELLS.

#### **COMMUNICATIONS:**

Name/Representing: JOE COKNS (SUB TO OVERSITE KR.)
Subject/Comments:

9:25 JOE WILL BE PROVIDING OVERSITE FOR TODAY'S WORK, NOTED THAT A REPRESENTITIVE FROM USEPA MAY ALSO STOP BY TODAY

QC'd By:	7117	2
	7	



#### **GENERAL NOTES**

PROJECT NAME: HOD ENGINEERING PO	DATE: ///09/99
PROJECT NUMBER:5314.04	AUTHOR: JAMES TINJUM
TIME ARRIVED ON-SITE: 6: 20	TIME LEFT SITE: 17:20

WEATHER: MOSTLY SUNNY, LIGHT BREEZE FROM SOUTHWEST AM: 59° F WHEN ARRIVED ON SITE

#### WORK/SAMPLING PERFORMED:

GAS, LEACHATE DEPTH, AND WELL DEPTH READINGS
AT THE FOLLOWING LOCATIONS: GWF & 3,4,5,6,7,8,12,13,
AND 14; LP& B AND 9; PZA, PB, AND PQ.

CONDUCTED WELL STICKUP MEASUREMENTS AND CONDITION
OF WELLS COVER OBSERVATIONS. RECORDED DEPTHS
PROBLEMS ENCOUNTERED/CORRECTIVE ACTIONS TAKEN: AND LEVELS IN MHE
AND MHW.

THE WAS OBSERVED ON PROPERTY APPROXIMATELY MILE SOUTHERST OF SITE, NO AFFECT ON FIELD INVESTIGATION.

#### **COMMUNICATIONS:**

Name/Representing: Row MURAWSKI USEPA

Subject/Comments: No Row NOTED THAT HE DIDN'T EXPECT US (RMT & WMI) TO MEET THE AGGRESSIVE RD SCHEDULE SET DUE TO REVIEW PROCESSES.

LOE CORNS - ON SITE FOR VEEPA OVERSIGHT

**REV 01/14/94** 



GENERA	L NOTES
PROJECT NAME:	DATE:
PROJECT NUMBER:	AUTHOR:
TIME ARRIVED ON-SITE:	TIME LEFT SITE:
WEATHER:	(September )
WORK/SAMPLING PERFORMED:	\$
PROBLEMS ENCOUNTEDED/CORDECTOR A CORD	
PROBLEMS ENCOUNTERED/CORRECTIVE ACTION	S TAKEN:
COMMUNICATIONS:	
Name/Representing:	
Subject/Comments:	
A STONE STATE OF THE STATE OF T	QC'd By:

# H.O.D. LANDFILL LANDFILL GAS AND LEACHATE MONITORING

Date: 11 08 199	Air Temperature: 60-70° °F
Field Technician: JAMES TINSUM	Atmospheric Barometric Pressure: in. Hg R/F
Signature: 10 Mes M. Tinjum	Weather Conditions: SUNNY & BREEZY
Q	Ground Conditions:
	Gas/O2 Meter Model: LANDTEC GMILL GEM 500
	Gas/O2 Meter Serial No.: EOBIZ
MIT	Date Last Calibrated: 10/22/91

Extraction Wells	% CH <sub>4</sub>	%: CHi LÊL	% O <sub>2</sub>	% CO <sub>2</sub>	Balance. Gas %	FLEL®	Depth to Leachate(1)	Well Depth(I)	Screen	Well Condition/Comments
LP1	3.5	20	. 2	1.6	75.2		11.3	12		
LP2	64.5	0.	.4	27.8	4.4		19.4	36'		,
LP3	14.4	17	.4	3.7	<i>45.7</i>		15.5	2 <b>8</b> ′		Y
LP4	67.2	Ō	.3	27.5	5.0		18.4	39'	·	
LP5	62.9	0.	4	33.8	2.9		57.0	53'		GAS VAPORS READILY OBSERVED WHEN CAP DEF
LP6	0.4	2	c.i	.2	18.5		11.9	<i>₹</i> %		
l P7	65.4	0.	0.	34.7	0.0		15.5	56'		

#### H.O.D. LANDFILL LANDFILL GAS AND LEACHATE MONITORING

Extraction Wells	% CH4	% CH4 LEL	% O <sub>2</sub>	% CO <sub>2</sub>	Balance Gas %	% LEL(2)	Depth to Leachate <sup>(1)</sup>	Well Depth(1)	Screen Interval	Well Condition/Comments
LP8	65.5°	A	6.4 0.4	278 37.5	4.4		32.2	65'	· ;	
LP9	03.5		0.0	36.4	0.0		21 4	67'		20' + OF LEACHATE DILY RESIDUE ON T.D.
LP10	66.6		0.4	25.6	6.0		14.1	26'		'
LP11	65.Z		0.2	30.2	4.4	L	18.8	31'		
LP12	9.5		0.2	24.7	4.6		20.1	25'		
LP13	34.5		11.8	12.5	39.8		15.8	(8		
LP14	69.7		0.0	26.1	4.2		19.5	24		CONDENS ATE NOTED
GWF1	<b>4.0</b>	k Topia	0. ).	32.7	3.\		33.4	42	13	PREVIOUS MENSUREMENTS
GWF2	G.0		0.3	32.9	3.0		30:8	48'	R	PREVIOUS MEASUREMENTS 30'9" TO LEACHATE 477" TO BOTTOM
GWF3	62.5		0.2	32.9	4.1		39.1	44'	20	+ LDTS OF POSITIVE PRESSURE IN WELL M. READING SAID 30'3"
GWF4	63.5		0.2	36.2	0.1		40.1	46'		PREVIOUS READING ON DUCT TRPE IS 39'10" - SUBSTANTIAL POSTING

#### H.O.D. LANDFILL LANDFILL GAS AND LEACHATE MONITORING

Extraction Wells	' % CH4	% CH4 LEL	% O <sub>2</sub>	% CO <sub>2</sub>	Balance Gas %	% LEL <sup>(2)</sup>	Depth to Leachate <sup>(1)</sup>	Well Depth <sup>(1)</sup>	Screen Interval	Well Condition/Comments
GWF5	45.2		6.1	26.2	22.4		26.1	46'		PREV. MERS. ZG' 4" TO LID. 45' 3" TD
GWF6	66.Z		0.2	33.0	0.7		19.3	41'		CAN HEAR GAS BUBBLING' IN PREJ. MERS: 19'7' + 41' T)
GWF7	64.5		1.3	29.5	3.5		30.7	48'		WELL PROBE COVERED WITH OILY RESIDUE WHEN
GWF8	16.8		15.4	9.4	58.4		18.5	45'		18'-8" TO BUTTOM
GWF9	62.5		0.6	33.4	3.5		3.3.7	47'		PROBE ; ON ROPE
GWF10	64.0	64.D.	0.1	33.5	2.5		27.1	42.5		WELL WAS DUCT TAPED
GIVF11	69.0		1.6	21.0	8.8		8.7	32'		(1) PREVIOUS MEAS. WAS 8'10"
GWF12	0.0		20.9	0.2	78.9		7.1	18'		NO PRESSURE BUILDUP MOTE
GIVF13	62.7	83	0.0	37.3	O.O		24.9	451:		PREVIOUS MEASUREMENTS LIGHTO @ 29' 44' 10" TO BUTTOM
GWF14	6l.B		0.1	38.1	0.0		24.7	39		CAN HEAR GAS BUBBLING IN VIGOROUSLY PREV. MEASUREMENT!

24' 4" TO WATER 38' 8" TO BOTTOM

T\WPMSN\PJT\00-05314\02\Z000531402-003 DOC 11/03/99

#### H.O.D. LANDFILL LANDFILL GAS AND LEACHATE MONITORING

Extraction Wells	% CH4	% CH4 LEL	% O <sub>2</sub>	% CO2	Balance Gas %	% LEL(2)	Depth to Leachate <sup>(1)</sup>	Well Depth(i)	Screen Interval	Well Condition/Comments
Pl	63.5		0.1	32.5	3,9		28.6	NM		
P2A	65.0		0.0	35.0	0.0		55.3	75±		UT INSIDE WELL $\phi = 334$ Thus could not get pic probe Down, measurement by them we
РЗА	63.0		0.1	36.9	0.0		31.2	65°		COULD NOT GET PVC. " PROBE DOWN BECAUSE PVC CASING IS 3"4"
P8	62.5		0.0	37.5	0.0		23.9	NM		
P9	0.4		20.6	0.3	78.7	, ,	13.4	42'		NO PUMPS OR ACCESSORIE DOWN HOLE
P10	6.9		1.91	3.1	71:2		27.0	NM		* NO WATER TO A, MAX. DEPTH OF 27'

Note:

NM = NOT ABLE TO MEASURE

<sup>(1)</sup> All depths are recorded from the top of the well casing.



9 OF 19

V44 Hearliand Trail P.O. Box 8923 Madison, WI 53708-8923 (608) 831-4444 FAX: (608) 831-3334

9:41 CALIBRATION OF LANDTEC

ZERD'D TO ATMOSPHERE + OK

ZERO'D COZ MA CHANGE

CHECK CH4 CALIBRATION TO CONTROL (15%)

READ 15.0% + OK

CHECK CO2 CALIBRATION TO CONTROL (15%)

READ 15.0% - OK

CHECK O2 CALIBRATION TO CONTROL (4%)

READ 3.9% - OK

10:05 (ALIBRATION OF 580B DVM

SPAN PPM = 0097 DX (READS 97.9 PPM)

ISOBUTYLENE @ 97 PPM)

10:30 BEGIN MEASUREMENTS AT GWF 10

10:55 ABRIVE AT LP 14 PHOTO 1

11:10 ARRIVE AT LP12-PHOTO 7

MARK TORRESAUL LEAVES SITE /

11:27 ARRIVE AT LP 13 PHOTO 3

11:46 ARRIVE AT LP 10
PHOTO 4



SHEET\_ P.O. Box 8923 Madison, WI 53708-8923 (608) 831-4444 FAX: (608) 831-3334

PROJECT / PROPOSAL NAME PREPARED

CHECKED PROJECT/PROPOSAL NO. DY MT 11/08/09 5717 HOD ENGINEERING PDI

ARRIVE AT LP3 11:59 PHOTO 5

12:20 BREAK FOR LUNCH

12:55 BACK ON SITE

13:05 ARRIVE AT LPA - PHOTO 6

13: 22 ARRIVE AT LPI - PHOTO 7

13:36 ARRIVE AT LP2 - PHOTO 8

13:54 ARRIVE AT LPII - PHOTO 9

CASING CAP IS 31/2 ELEVATED 14:09 ARRIVE AT PID - PHOTO 10

14:30 ARRIVE AT GWF 11 - PHOTO 11

14:46 ARRIVE AT LPG - PHOTO 12

15:10 ARRIVE AT GWF 9 - PHOTO 13

15:29 ARRIVE AT LPS - PHOTO H

15:44 ARRIVE AT GWF1 - PHOTO 15

16:01 ARRIVE AT GWFZ - PHOTO 16

16:15 ARRIVE AT PI - PHOTO 17

16:24 ARRIVE AT GWF3 - PHOTO 18

16.36 JOE CORNS NEEDS TO LEAVE SITE,

I NOTE THAT I WILL CLEAR UP AND DECON. FOR REMAINDER OF DAY

17:05 LEAVE SITE TO PURCHASE LOCK FOR FRONT GATE

18:00 APPLY NEW LOCK, LEAVE SITE, - END OF DAY-



P.O. Box 8923 Madison, WI 53708-8923 (608) 831-4444 FAX. (608) 831-3334

PROJECT / PROPOSAL NAME HOD ENGINEERING PDI

CHECKED PREPARED PP TML TO

6: 40 CALIBRATE LANDTEC

ZERO'D PRESSURES - DK

CH4 ZERO'D - OK

CH4 SPAN (15.0%) - READS 15.0% OK

CO2 SPAN (15.0%) - READS 14.9% OK

D, ZERO'D - OK

0, SPAN (4.0%) - READS 4.0% OK

MEASURE BACKGROUND CONCENTRATIONS

CH4 0.0%

الص

02 20.9%

BAL 79.0%

6:59 CALIBRATE 580B OVM

RF = 1.0

LAMP = 10.UeV

RESET TO ZERO GAS - OK

USE 97 ppm ISOBUTY LENE SPAN GAS

SPAN CALIBRATION OK

CHECK LANDFILL BACKGROUND

000.5 PPM MAX OK

7:13 FARRIVE AT GWF 12 - PHOTO 19

7:35 PARIVE AT GWF 8 - PHOTO 20

7:49 ARRIVE AT LP7- PHOTO 21

8:05 PHOTO OF GWF3 (#22)

- DUTWARD PRESSURE BULGING DUCT TAPE

SHEET.

Madison, WI 53708-8923 (608) 831-4444 FAX: (608) 831-3334

PROJECT / PROPOSAL NAME HOD ENBINEERING PDI

P.O. Box 8923

PREPARED By DayMT By: T Date: | Octo

CHECKED

Z

PROJECT/PROPOSAL NO. 53 H . D4

ARRIVE AT PZA - PHOTO 23 8:09

I.D. OF PUC WELL IS 34"

8:29 ARRIVE AT GWF4 - PHOTO 24

8:44 OVERSITE KR APRIVES, JOE CORNS

8:49 ARRIVE AT LPB - PHOTO 25

9:02 ARRIVE AT GWF 13 - PHOTO 26

- CAM HEAR' GAS BUBBLING INTO WELL

- HERVY FOSITIVE PRESSURE

9:19 ARRIVE AT GWF 14 - PHOTO 27

9:35 RON MURAWSKI ARRNED ON SITE

DISCUSSED GENERAL PROCEDURES. WHAT HAS BEEN DONE TO DOTE,

REMEDIAL SCHEDULE & ACCESS AGREEMENTS

9:57 PARIVE AT 189- PHOTO 28

BROWNISH, DILY RESIDUE ON ROPE USED TO MEASURE TOTAL DEPTH, PUC PIPE USED ALSO CIATED.

10:19 ARRIVE AT GWF 6 - PHOTO 29

ARRIVE AT GWF5 - PHOTO 30 10:37

MEASURED BREATHING ZONE

0.0 PPM BY OVM 580 B

11:04 ARRIVE AT P3A - PHOTO 31

11:26 ARRIVE AT P8 - PHOTO 32,33

11:39 ARRIVE AT PG - PHOTO 34 (PHOTO NOT TAKEN)

11:55-12:45 LUNCH WITH RON MURAWSKI AND JOE CORNS



<u>고</u> /	ישער.	<i></i>			SHEET	13	OF	1
		0.0.0	Mades - MI 50700 0000	(500) 631 4444	EAV. (COO) 004 0004			

44 Heartland Trail P.O. Box 8923 Madison, WI 53708-8923 (608) 831-4444 FAX: (608) 831-3334

PROJECT / PROPOSAL NAME

HOD ENGINEERING PDI

THAT DINN DYN - DOIS 10 5314.04

12:55 ARRIVE AT GWF-7 - PHOTO 3534 WILL
HES OVM REDDING IN
BREATHING ZONE = 0.5 PPM

- 13:16 BEGIN WELL STICKUP AND CONDITION OBSERVATIONS
  - GWF7 3'9%" TO FLARE FLANGE
    FLARE RUSTED BUT NOT DEGRADED, SURROUNDING
    COVER IN GOOD CONDITION
- 13:20 GWFB 3'O' TO FLARE FLANGE
  POSITIVE PRESSURE, SOME CONDENSATE DRIPS,
  FLARE RUSTED, FLAME BUCKET CRACKED,
  BRITTLE, NOT HEAVILY CORRODED, COVER IN
  600D CONDITION
- 13:25 TPZA 3'71/2" TO 6" STEEL CASING TOP

  PVC 51/2" BELD W CASING TOP (35/4" ID)

  SURFACE GROUT/CONCRETE BROKEN,

  COVER IN GOOD CONDITION
- 13:29 GWF 4, HERVY POSITIVE PRESSURE
  2'64" TO FLARE FLANGE

FLARE BUCKET CRACKED WITH WHITE RESIDUE
FLARE COATED W GREY BLACK RESIDUE
SOME STRESSED VEGETATION, OTHERWISE GOOD COVER 13

13'33 + LPE Z'II'' TOP CASING (RUSTING CORRUSION)

9" PLUS TO TOP PUC (NO PUC CAP)

FEW DEPRESSED HOLES (1-2' &) NEARBY, APPRUX 6"DEPRESSED



SHEET	OF

744 Heartland Trail P.O. Box 8923 Madison, WI 53708-8923 (608) 831-4444 FAX. (608) 831-3334

FROJECT / PROPOSAL NAME

FROD ENGINEERING PD/

PREPARED CHECKED PROJECT / PROPOSAL NO.

5314.04

13:38 → GWF 13 3'5½" TO FLARE FLANGE DRIP COATING ON PVC FLARE SLIGHTLY RUSTED, FLARE APRESTOR CRACKED BROKEN

COVER CRACKED AT PUC SURFACE ENTRANCE

13:41 GWF 6 3'6' TOP OF FUC (BROKEN OFF SLIGHTLY BELOW FLARE FLANGE

TILTED ~ 100

COVER IS LOW WITH STANDING WATER AND

FLARE HEAVILY AUSTED, FLARE ARRESTOR RUSTED CORROLDED

13:45 GWF 15 A 2'44" TO FLARE FLANGE COVER IN GOOD CONDITION FLARE WI SOME RUST, ARRESTOR RUSTED CORRODED

13:47 LP 9 2'5" TO TOP CASING (RUSTED)
51/2" PLUS TO PUC TOP

CASING HAS SETTLED, SURFICE CRACKS OTHERWISE, COVER WELL VEGETATED

13:50-FGWF 5, SOME DRIPS ON PUC 3'4" TO TOP OF PUC FLARE SLIGHTLY RUSTED ARRESTOR CRACKED CORRODED HEAVILY COVER DEPRESSED TO SOUTH SLIGHTLY

13:53 P3A 4'314" TOP OF STEEL CASING WHICH SITS LODSE AT GRADE (SURFACE SEAL POOR)
44" MINUS TO TOP PVC, COVEROK



רי <u>חחח</u> *		SHEET	15	of 19
74444 4 47 4 8 8 8 8 8 8	 10001 001 1111	EAV (COO) 004 0004		

PROJECT / PROPOSAL NAME

HOD ENGINEERING FOIL DOG 5314.04

14:00 - P1

EXTRACTION POINT WITH CORRUGATED STEEL MANHOLE
ESI LIQUID LEVEL INDICATOR
STEEL CABLE PULLEY
3' 3" STICKUP (TOP PVC)

DOWNHOLE IS LEACHATE LINE (14" OD)

AIR LINE (7,00)

3/4" PZ (PVC) LINE ELECTRIC LINE (?)

INSULATION HERVILY DETERIORATED

LEACHATE

MHI

CULVERT

CULVERT

AT GRADE

D 11

D 12

3 RAYCHEM CHEMFLEX AUTO-TRACE PARALLEL SELF REGULATING HEATER

14:11 → GWF Z 1'7" PUC STICKUP (ORANGE/RED STAINED)
FLARE AND ARRESTOR RUSTED
3'\$\phi\$ BARE SPUT AROUND WELL

14:14 - GWF8 1'64" PUC STICKUP (NOT STAINED)

FLARE RUSTED, ARRESTOR IN GOOD CONDITION
COVER IN GOOD CONDITION

14:16 - LP7 2'9'4" TO TOP CASING

PLUS 1'6" TO TOP PVC LOW N-S SWALE 15't TO WEST PVC ORANGISH TINT WELL CASING AREA HAS SETTLED

Madison, WI 53708-8923 (608) 831-4444 FAX. (608) 831-3334

PROJECT / PROPOSAL NAME CHECKED PREPARED

HOD ENGINEERING FDI

14:20 GWES 1'7" PUC STICKLE (NO STAINING) FLARE AUSTED PREPETION IN GOOD CONDITION COVER IN GOOD CONDITION

4:23 PHOTO 3435 F N

ELECTRIC POLE SETWEEN SHED & GWF !

14:26 - GWF 11 2'10'2" PVC STICKUP (NOT STAINED) FLARE RUSTY, ARRESTOR ONLY SLIGHTLY RUSTEN COVER IN GOOD CONDITION

14:28 + LP6 3'6" TO TOP CASING PIUS 14" TOP PUC MINOR STAINS, STEEL CASING RUSTEL CASING SLIGHTLY DEPRESED, OTHERWISE COVER IN GOOD CONDITION

14:31 - GWF9 2' 41/4" TO FLANGE PUC WELL STAINED (ORANGE RED) FLARE RUSTY , NO ARRESTOR OBSERVED COVER IN GOOD CONDITION

14:33 - LP5 3'64" TOP CASULO MINUS 12" TOP PUC

> CASING HAS ORANGE STAINED DRIPS TO GROUND, COVER VEGET: IN GOOD CONDITION

14:36 - GWF 6 1'5% FLANGE FLARE ARRESTOR HEAVILY CORRODED, CRACKED COVER SLIGHTLY DETRESED, VEGETATION GOOD

14:39 PHOTO 367 36 Km MAJOR FIRE SMOKE PLUME SE OF SITE

P VIII INC	COMP	PUTATION	N SHEET		
744 Hearland Trail P.O. Box 8923 Madison, WI 53708-8923 (608)	SHEE T 831-4444	17	of 19		
PROJECT/PROPOSAL NAME HOD ENGINEERING PD1	PREPARED CHECKET		PROPOSAL NO.		
15:02 FROM RADIO 5-ALARM BRUSH FIR	Æ TO SW.	OFF OF	HWY I		

73 NOTED TO JOE THAT IF I SAW ANY HINTS OF FIRE, I WAS GOING TO ABANDON SITE FOR DAY 15:04 + PB EXTRACTION POINT WITH CORRUGATED STEEL MANHOLE

2' 9/2" TO CASING TOP PLUS 834" TOP PVC

COPI

HAS DZ, LEACHATE, AND AIR DOWN HOLE PLUS CABLE

15:10 - PO No LINES GOING DOWN HOUSE CABLE PULLEY INPLACE LINES ANN TO SOUTH (AT GRADE) 5'94" TOP CASING (HEAVILY RUSTED) PLUS 4" TOP PVC

15:16 - GWF 12

2' 1" TO TOP PIC STICKUP (SOME ORPHUSE DISCOUDRING) FLARE AND ARRESTOR BOTH LIGHTLY RUSTED LOW WET AREA SOUTH AND WEST (OTHERWISE CONES UND LEGELYLLION GOOD

AT GRADE LEACHATE LINE RUNS 15' TO SOUTH 15:20 -P 10 CABLE, LEACHATE, AND ARE HEATING DOWNHOLE

2'0" TOP CASING KINKED PLUS TO TOPPIC

#### COMPUTATION SHEET



			SHFFT	18	of 19	
244 Handland Trail B.O. Pay 8022	Madison W/ 53708.8023	(608) 831 4444	EAY (608) 831 3334			

PROJECT / PROPOSAL NAME

15:25 - GWF 10 1'4" PVC STICKUP (ORANGE STAINED FLARE AND ARRESTOR RUSTED (EXCEPT BOTTOM SECTION) COVER IN GOOD CONDITION, TWO SMALL TREES 20' WEST

15:30 - LPI 2'9" TOP CASING.

PLUS 44" TOP PVC

DEPRESSION IMMEDIATELY AROUND STEEL CASING, OTHERWISE COVER GOOD

15:33 F W, NW PHOTOS Ø.1,2

ELECTRIC POWER COMING TO SITE

15: 35 + LP 4 2'5" CASING STICKUP

- 1 1/2" TO PUC TOP (STAINED GREY)

COVER IN GOOD CONDITION

15:37 - LPZ 2'5½" CASING STICKUP (RUSTED)

+ 34" PVC TOP

COVER IN GOOD CONDITION

15:40-15:48 JOE CORNS LEAVING

- NOTED THAT PDI WENT PER WORKPLAN AND

HE WILL RELAY THAT TO WESTON AND ETA.

15:51 - LPI 3'34" CASING STICKUP

- 31/2" TOP PUC (CLEAN)

COVER GOOD, CASING SUGHTLY DEPRESSED

15:56 LP3 3'4" CASING STICKUP (SLIGHTLY DEPRESES)

GOOD VEGETATION PVC

15:58 LPID 3'14" (ASING STICKUP & GOOD VEGETATION)

16:00 LPB 2'9" CASING ? PVC STICK UP (CLEAN) 18 GOOD VEGETATION

2' 3"4" CASING STICKUP 1602 LP12 34" TO TOP PUC (ORANGE ST ALMED)

CORRSE SAND AROUND CASING AT BASE

16:05 LP 14 2'8" TOP CHEING

11/2" TO TOP PVC (CLEAN)

CORRESE SAND SEAL IS SLIGHTLY DEPRESSED,

OTHERWISE VEGETATION GOOD

ML:12 MHW PHOTO 3

26.5' TO LEACHATE FROM CONCRETE RING TOP - 2'0" TO GRADE

2' 1" MANHOLE SECTIONS 34' TOTAL DEPTH

16:19 EMH PHOTO 4,5

23.6' TO LEACHATE FROM MH TOP

- 2'0" TO GRADE 37.5' TOTAL DEPTH

# Appendix B Photographs



Roll 1, Photograph 30, Facing Northeast 11/09/99 at 10:37, View of GWF 5



Roll 1, Photograph 18, Facing Northeast 11/08/99 at 16:24, View of GWF 3





Roll 1, Photograph 13 Facing Northeast 11/08/99 at 15:10 View of GWF 9

Roll 1, Photograph 6 Facing Northwest 11/08/99 at 13:05 View of LP 4



Roll 1, Photograph 17, Facing Down 11/08/99 at 16:15, View of P1



Roll 1, Photograph 33, Facing Southeast 11/09/99 at 11:26, View of P8



Roll 2, Photograph 4, Looking Down 11/09/99 at 16:19, View Down Eastern Manhole



Roll 2, Photograph 5, Facing Northwest 11/09/99 at 16:19, View of Leachate Storage Tank and Appurtenances

# Appendix C Well Construction Details

#### TABLE 1-5 SUMMARY OF MONITORING WELL CONSTRUCTION DETAILS H.O.D. LANDFILL ANTIOCH, ILLINOIS

Well	Completion	Coord	inates	Ground	TOIC	Total	Well/Screen	Screen	Stratigraphy	Top of Sa	nd Pack	Scre	en Inte	rval	Scree	n Int	erval
#	Date	North	East	Elev	Elev	Depth	Materials	Length	at Screen	Depth	Elev		Depth		Ele	evatio	on
																l	
EPA V	Vells												]		]	l	
USIS	5/22/87	2115302.72	1053552.35	766.5	768.69	12.41'	stainless	5.7'	silty sand & gravel	3.50	763.00	6.71	to	12.41	759.79	to	754.09
USID	5/27/87	2115302.79	1053547.83	766.9	768.88	92.41'	stainless	5.7'	f-med Sand	81.00	685.90	92.41	to	86.71	674.49	10	680.19
US2D	6/16/87	2114832.02	1050654.41	768.2	770.73	112.77'	рус	8.3'	sand & gravel	103.00	665.20	104.47	lo	112.77	663.73	to	655.43
US3S	6/2/87	2115488.87	1050515.19	767.1	770.48	22.5'	stainless	5.7'	sand & gravel	13.50	753.60	16.81	to	22.51	750.29	to	744.59
US31	6/10/87	2115483.04	1050532.52	767.01	769.93	58'	pvc	3,	CL to SC	52.50	714.51	55	10	58	712.01	to	709.01
US3D	6/3/87	2115486.53	1050523.96	767.1	769.72	83'	pvc	5.3'	fine-med sand	73.50	693.60	77.28	10	82.58	689.82	to	684.52
US4S	6/17/87	2115388.68	1050754.78	771.1	773.67	23'	stainless	5.7'	sand & gravel	15.00	756.10	17.17	10	22.87	753.93	to	748.23
US4D	6/23/87	2115377.82	1050754.38	770.5	772.7	103.84	stainless	5.7	fine-med. silt	94.00	676.50	98.14	to	103.84	672.36	to	666.66
US5D	6/29/87	2116743.35	1050757.09	765.1	767.73	93.14'	stainless	5.7'	sand & gravel	84.00	681.10	87.44	lo	93.14	677.66	to	671.96
US6S	7/10/87	2115367.32	1051516.03	767.1	769.9	41.7'	stainless	5.7'	sand & gravel	NA	NA	36	10	41.7	731.1	10	725.4
US6I	7/10/87	2115380.91	1051520.35	767.6	770.21	62.76	stainless	3.7'	CL	55.00	712.60	59.06	lo	62.76	708.54	to	704.84
US6D	7/6/87	2115387.72	1051523.28	767.1	770.09	83.17'	stainless	5.7'	sand & gravel	74.50	692.60	77.47	10	83.17	689.63	lo	683.93
US7S	7/16/87	2116603.79	1051803.25	764.4	767.99	32.63'	stainless	5.7'	Interbedded Cl+GP	25.00	739.40	26.93	to	32.63	737.47	10	731.77
TSC We	lls																
GHS	NA	2116538.48	1050747.65	767.6	770.12	NA	NA	NA	fine to coarse sand	NA	NA	NA		NA	NA		NA
GIID	NA	2116541.35	1050747.19	767.1	769.99	NA	NA	NA	organic silty clay	NA	NA	NA		NA_	NA		NA
G14S	5/7/74	2115621.98	1053289.24	767.6	770.34	10	NA	NA	clayey sand	NA	NA	NA		NA	NA		NA
GI4D	5/7/74	2115619.37	1053288.07	767.7	769.75	34	NA	NA	silty sand	NA	NA	NA		NA	NA		NA
G102	5/8/74	2115417.06	1050750.06	771.1	773.53	25	NA	NA	f-c sand	NA	NA	NA		NA	NA		NA
R103	10/31/85	2115400.27	1051520.55	767.6	769.55	27	pvc	5	f-c sand tr. gravel	17.7	NA	21	10	27	746.6	to	740.6
														<u></u>	<b> </b>	Ī	
TSC Lea	achate Wells													<b>.</b>	<b>!</b>		
LPI	5/19/83	1+80S	13+35W	797.73	N/A	45	PVC	30	Fill and Refuse	4.5	792.8	13	to	43	784.3	lo	754.3
LP8	5/20/83	6+50S	5+00W	796.23	N/A	43.5	PVC	30	Fill and Refuse	4	792.93	13	to	43_	783.93	10	753.93
LP9	5/20/83	6+50S	10+00W	795.06	N/A	43.5	PVC	30	Fill and Refuse	4	791.06	13	to	43	782.06	to	752.06
LP10	5/23.83	7+50S	14+50W	795.06	N/A	45	PVC	30	Fill and Refuse	4	791.06	13	to	43	782.06	10	752.06
P2A	9/18/84	1+80S	10+00W	795.1	797.6	15	PVC	65	Fill and Refuse	4.5	790.06	6.6	lo	71.6	788.5	to	723.5
P3A	9/21/84	I+80S	5+05W	792.4	794.7	75	PVC	65	Fill and Refuse	5	787.4	7.7	to	72.7	784.7	10	719.7
	L						<b></b>	1								_	
Warzyn	Wells		<u> </u>			]						l	]	l		1	
W2D	4/20/93	2116648.18	1052499.88	770.7	773.04	88.33'	pvc	5,	f-c sand	79.80	690.90	83.3	10	88.3	687.4	10	692.4
W3SA	4/7/93	2115185.28	1051029.19	763.8	766.54	15.64	pvc	10.09	f-c sand	5.00	758.80	5.55	to	15.64	758.25	to	748.16
W3SB	4/7/93	2115189.39	1051027.83	763.7	766.81	29.57	pvc	5'	sand over. clay	22.55	741.15	24.55	to	29.57	739.1	to	734.13

PMS/gmg/TAB/DAP/SJC/jrs/ j.\10010202\wp\\b\\99HODWLS XLS

TABLE 1-5
SUMMARY OF MONITORING WELL CONSTRUCTION DETAILS
H.O.D. LANDFILL
ANTIOCH, ILLINOIS

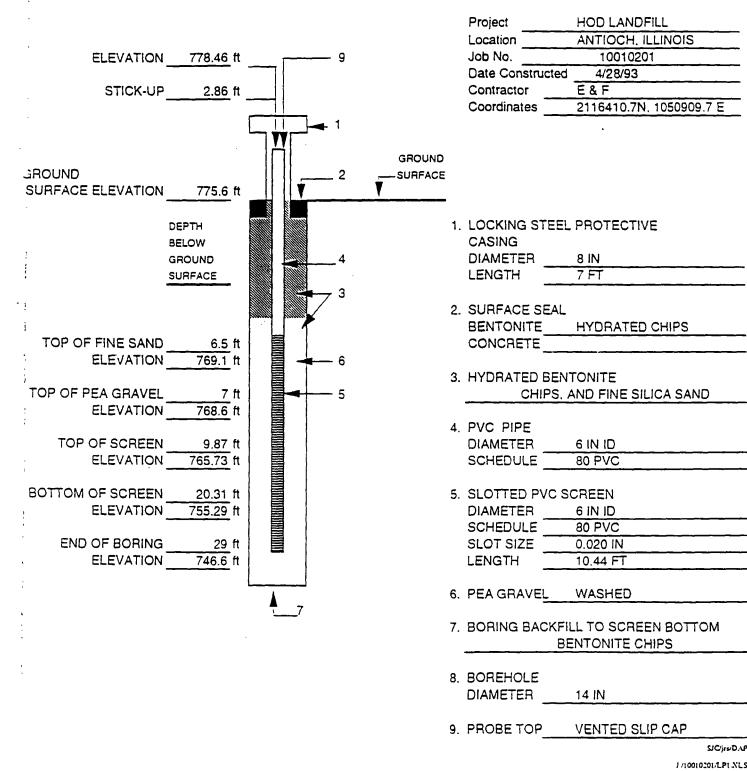
Well	Completion	Coord	inates	Ground	TOIC	Total	Well/Screen	Screen	Stratigraphy	Top of Sa	nd Pack	Scree	en Inte	rval	Scree	n Int	crval
#	Date	North	East	Elev	Elev	Depth	Materials	Length	at Screen	Depth	Elev		Depth		Ele	evatio	on
W3D	5/25/93	2115187.6	1051022.66	763.73	765.93	78'	pvc	5'	f-c sand	70.90	692.83	73.3	to	77.6	690.43	lo	686.13
W4S	5/26/93	2115201.97	1050628.33	767.5	769.97	15'	pvc	10,	f-c sand	4.00	763.50	5	to	15	762.5	to	752.5
W5S	4/21/93	2115375.15	1050760.47	771.1	773.49	14.34	pvc	10.46	f-c sand	3.90	767.20	5.22	to	14.34	765.88	to	756.76
W6S	4/16/93	2115399.38	1051541.09	764.9	767.41	15'	pvc	9.18'	f-c sand	4.00	760.90	5.82	to	15	759.08	to	749.9
W7D	4/14/93	2116325.98	1053153.28	780.2	782.87	99.72	pvc	4.3'	f-c sand	93.00	687.20	95.42	10	99.72	684.8	10	680.48
W8D	3/21/93	2115325.82	1052660.77	766.68	768.14	94'	pvc	5'	f-c sand	76.60	690.08	89	lo	94	677.68	to	672.68
PELA Pi	ezometers														L1		
PZI	8/10/89	2116820.66	1053361.37	786.2	788.48	118.2	stainless	10'	clay over sand	102.00	684.20	108.2	10	118.2	678.2	lo	668
PZIU	2/28/90	2115026.24	1051398.67	763.9	766.41	27'	pvc	20'	sand	5.50	758.40	7	to	27	756.9	lo	736.9
PZ2U	3/1/90	2114903.68	1050856.51	764.1	768.04	16.5'	pvc	10'	sand	5.00	759.10	6.5	to	16.5	757.6	lo	747.6
PZ3U	3/5/90	2115540.75	1051908.41	763.4	766.27	37'	pvc	30'	sand	5.00	758.40	7	to	37	756.4	lo	726.4
PZ4U	3/6/90	2115619.7	1052359.45	763.3	766.49	27'	pvc	20'	sand & gravel	6.00	757.30	7	to	27	756.3	to	736.3
PZ5U	3/7/90	2115771.83	1053088.12	769.3	771.11	32'	pvc	20'	sand	10.00	759.30	12	to	32	757.3	lo	737.3
PZ6U	4/26/90	2115818.07	1052491.73	763.6	766.54	42.5	pvc	10'	sand & gravel	23.00	740.60	32.5	lo	42.5	731.1	to	721.1
																<del>                                     </del>	
PELA S	equoit Creek	Piezometers		<u> </u>												t	
SC-1A	3/4/90	2115370.25	1052636.44	764.7	766.84	13.2	1.25" Galvan.	5	silt/f-med. sand	5.00	759.70	8.2	to	13.2	756.5	10	751.5
SC-1B	3/2/90	2115325.82	1052637.67	766.4	769.34	23.69	1.25" PVC	10	silt/f-med. sand	7.50	758.90	13.69	to	23.69	752.7	10	742.71
SC-1C	2/28/90	2115254.06	1052641.84	762.9	765.44	15.55	1.25" PVC	5	sìlt/f-med. sand	10.80	752.10	10.55	to	15.55	752.3	10	743.14
SC-ID	2/28/90	2115231.17	1052643.06	762.94	766.39	19.8	1.25" PVC	5	f-v. coarse sand	13.90	749.04	14.8	to	19.8	748.14	to	
SC-2A	3/1/90	2115338.69	1051601.5	763.2	765.09	11.1	1.25" PVC	5	silt/f-coarse sand	5.70	757.50	6.1	to	11.1	757.1	to	752.1
SC-2B	3/1/90	2115316.07	1051603.37	766	767.24	19.1	1.25" PVC	5	f-coarse sand	3.37	762.63	14.1	to	19.1	751.9	to	746.9
SC-2C	2/22/90	2115260.1	1051600.09	763.2	764.51	14.9	1.25" Galvan	5.9	silt/f-c sand	8.75	754.45	9	10	14.9	754.2	to	748.3
SC-2D	2/23/90	2115241.45	1051600.63	763.4	764.77	13.7	1.25" Galvan	. 5	Cl/f-c sand	9.00	754.40	8.7	10	13.7	754.7	to	749.7
SC-3B	3/7/90	2115369.02	1050754.32	769.9	770.6	16.9	1.25" Galvan	5	f-c sand	8.46	761.44	11.9	10	16.9	758	to	753
SC-3C	3/20/90	2115358.14	1050690.91	767.7	770.26	15.5	1.25" Galvan	5	f-c sand/gravel	7.00	760.70	10.5	lo	15.5	757.2	to	752.2
SC-3D	3/20/90	2115359.75	1050673.05	767.1	769.77	15.5	1.25" Galvan	5	silt/f-c sand	8.00	759.10	10.5	10	15.5	756.6	to	751.6
SC-4A	3/7/90	2116552.59	1050772.28	768.8	770.22	27.5	1.25 " PVC	10	silty clay	15.00	753.80	17.5	lo	27.5	751.3	to	741.3
SC-4B	3/6/90	2116550.92	1050752.8	768.1	770.44	27.89	1.25 " PVC	10	clayey silt	17.44	750.66	17.89	to	27.89	750.2	to	740.21
SC-4C	3/5/90	2116539.91	1050689.83	765.8	768.53	17.3	1.25 " PVC	10	silt/fine sand	3.20	762.60	7.3	to	17.3	758.5	to	748.5
SC-4D	3/19/90	2116551.85	1050676.6	766.3	769.6	22	1.25 " PVC	10	silt/gravel	7.00	759.30	12	to	22	754.3	to	744.3

# TABLE 1-5 SUMMARY OF MONITORING WELL CONSTRUCTION DETAILS H.O.D. LANDFILL ANTIOCH, ILLINOIS

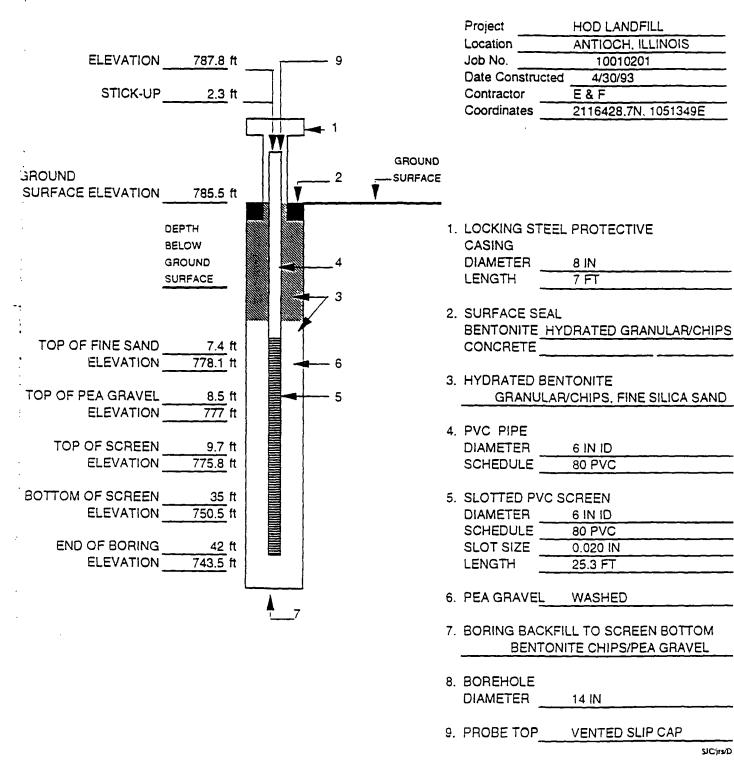
Well	Completion	Coord	inates	Ground	TOIC	Total	Well/Screen	Screen	Stratigraphy	Top of Sa	nd Pack	Scre	en Inte	rval	Scree	n Int	erval
#	Date	North	East	Elev	Elev	Depth	Materials	Length	at Screen	Depth	Elev		Depth		Ele	evatio	yn )
Warzyn	Gas Probes																
GP3	4/21/93	2116615.46	1052220.9	770.8	773.51	20	2" PVC	14.82	silty clay	3.6	767.2	5.03	to	19.85	765.77	10	750.95
GP4A	4/15/93	2116248.07	1053013.74	776.4	778.87	26	2" PVC	20.2	silty clay	5	771.4	5.8	lo	26	770.6	to	750.4
GP5A	4/22/93	2115682.26	1051583.29	768.4	770.8	16.1	2" PVC	10.1	silty clay	6	762.6	6	lo	16.1	762.4	10	752.3
Warzyn	Leachate Pie	zometers															
LPI	4/27/93	2116410.72	1050909.73	775.6	778.46	20.31	6" PVC	10.44	fill and refuse	7	768.6	9.87	lo	20.31	765.73	to	755.29
LP2	4/30/93	2116428.68	1051349.01	785.5	787.8	35	6" PVC	25.3	fill and refuse	8.5	777	9.7	to	35	775.8	to	750.5
LP3	4/28/93	2116082.67	1050918.94	778.1	780.89	22.5	6" PVC	14.5	fill and refuse	9	769.1	_!!_	lo	25.5	767.1	to	752.6
LP4	5/4/93	2116110.56	1051338.6	788.9	790.84	39	6" PVC	29.1	fill and refuse	8.6	780.3	9.9	to	39	779	to	749.9
LP5	4/21/93	2116229.99	1051719.62	796.6	800.13	50	6" PVC	39.5	fill and refuse	9	787.6	10.5	to	50	786.1	to	746.6
LP6	4/16/93	2115990.18	1051732.08	794.6	797.32	36.5	6" PVC	26.8	fill and refuse	8	786.6	9.7	to	36.5	784.9	10	758.1
LP7	4/28/93	2116197.77	1052105.4	794.7	797.39	61	6" PVC	51.5	fill and refuse	8.5	786.2	9.5	to	61	785.2	lo	733.7
LP8	4/27/93	2116218.62	1052519.39	793.5	796.35	70	6" PVC	60	fill and refuse	9	784.5	10	to	70	783.5	to	723.5
LP9	4/23/93	2116220.42	1052769.86	785.8	789.16	66.5	6" PVC	57.3	fill and refuse	8.5	777.3	9.2	to	66.5	776.6	10	719.3
LP10	4/27/93	2115810.43	1050919.77	781.1	783.92	23	6" PVC	13.5	fill and refuse	8.3	772.8	9.5	to	23	771.6	to	758.1
LPII	4/12/93	2115807.09	1051321.81	787.8	790.61	29.2	6" PVC	21.7	fill and refuse	7.5	780.3	9.3	lo	29.2	778.5	lo	758.6
LP12	4/8/93	2115515.46	1051138.39	782.6	784.85	22.5	6" PVC	12.5	fill and refuse	8	774.6	10	to	22.5	772.6	to	760.1
LP13	4/13/93	2115448.41	1050899.85	779	781.68	17	6" PVC	7.17	fill and refuse	9	770	9.83	to	17	769.17	lo	762
LP14	4/13/93	2115474.47	1051389.52	781.7	784.27	22.5	6" PVC	12.3	fill and refuse	8.9	772.8	10.2	to	22.5	771.5	to	759.2
Kelletts	Well Boring,	Inc.		1						,							
					1					I							
GWFI	6/23/88	2+63S	17+75W	795	798	42	8" PVC	22	fill and refuse	14	781	20	to	42	773	lo	751
GWF2	6/22/88	2+28S	14+86W	796.2	799.2	47	8" PVC	27	fill and refuse	17	779.2	20	10	47	776.2	to	749.2
GWF3	6/22/88	2+32S	11+49W	797.2	800.2	45	8" PVC	25	fill and refuse	17	780.2	20	10	45	777.2	to	752.2
GWF4	6/22/88	2+27S	8+55W	795	798	45	8" PVC	25	fill and refuse	17	778	20	10	45	775	10	750
GWF5	6/22/88	2+115	5+37W	789.2	792.2	55	8" PVC	35	fill and refuse	17	772.2	20	lo	55	769.2	to	734.2
GWF6	6/23/88	3+78S	7+47W	791.2	794.2	41	8" PVC	21	fill and refuse	17	774.2	20	to	41	771.2	to	750.2
GWF7	6/24/88	3+90S	10+70W	795.9	798.9	48	8" PVC	28	fill and refuse	17	778.9	20	to	48	775.9	to	747.9
GWF8	6/24/88	4+46S	14+50W	797.4	800.4	48	8" PVC	28	fill and refuse	17	780.4	20	to	48	777.4	lo	749.4
GWF9	6/25/88	4+945	16+72W	797	800	47	8" PVC	27	fill and refuse	17	780	20	to	47	777	to	750
GWF10	6/25/88	6+87S	17+59W	792.7	795.7	38	8" PVC	18	fill and refuse	17	775.7	20	to	38	772.7	to	754.7
GWFII	6/24/88	6+695	15+85W	793.6	796.6	40	8" PVC	20	fill and refuse	17	776.6	20	to	40	773.6	to	753.6
GWF12	6/24/88	6+20S	12+93W	792.5	795.5	22	8" PVC	10	fill and refuse	10	782.5	12	lo	22	780.5	to	770.5

PMS/gmg/TAB/DAP/SIC/jrs/ j:\10010202\wp\tbl\99HODWLS XLS



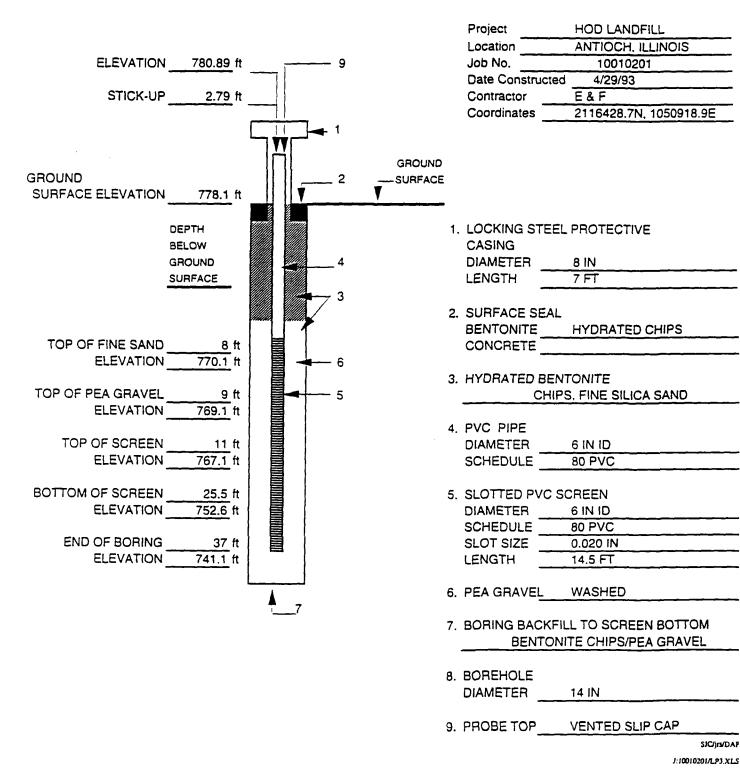




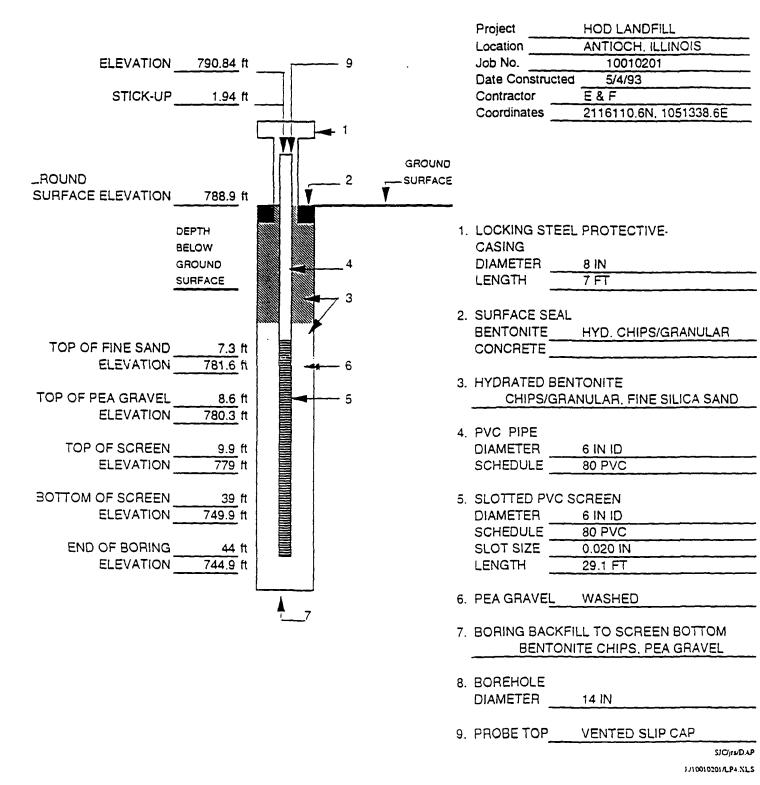


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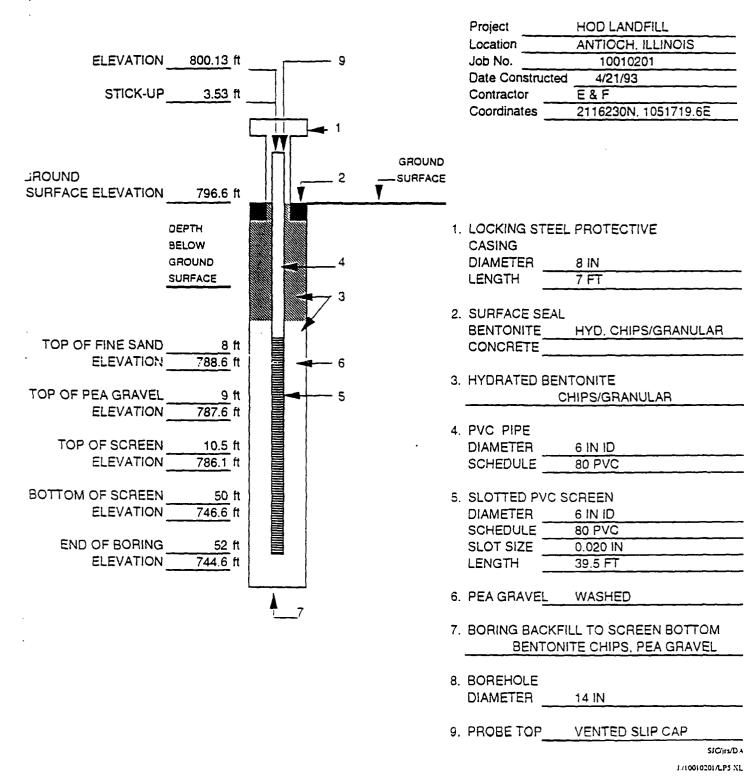




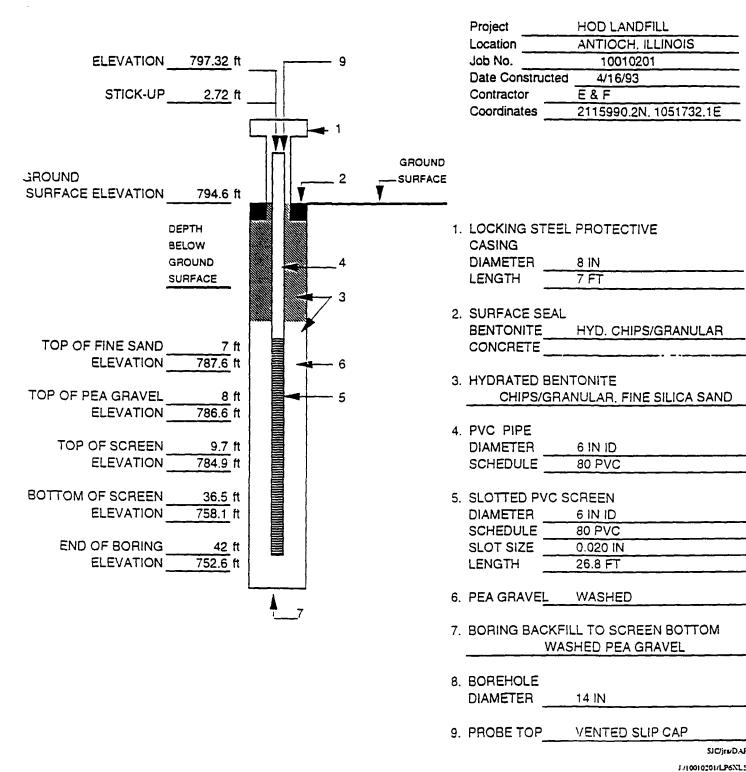




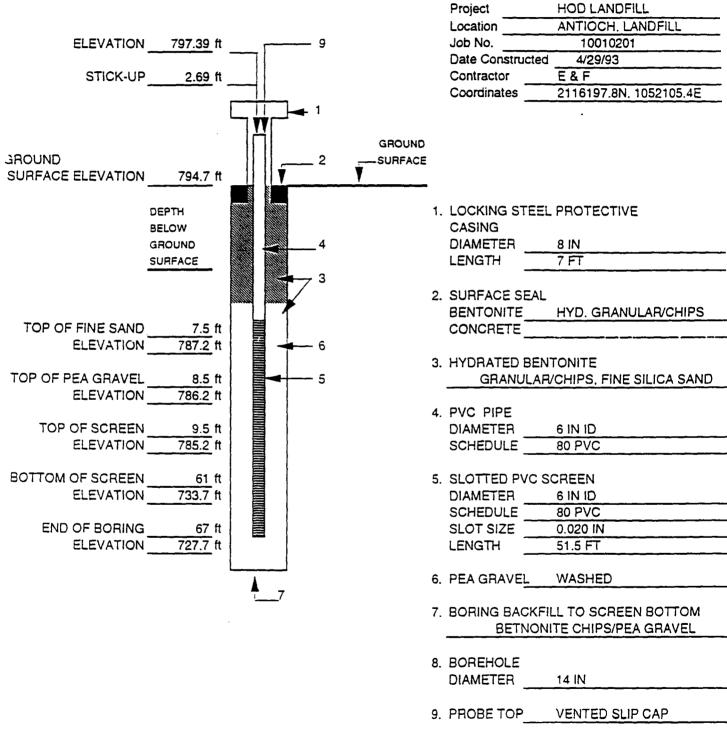








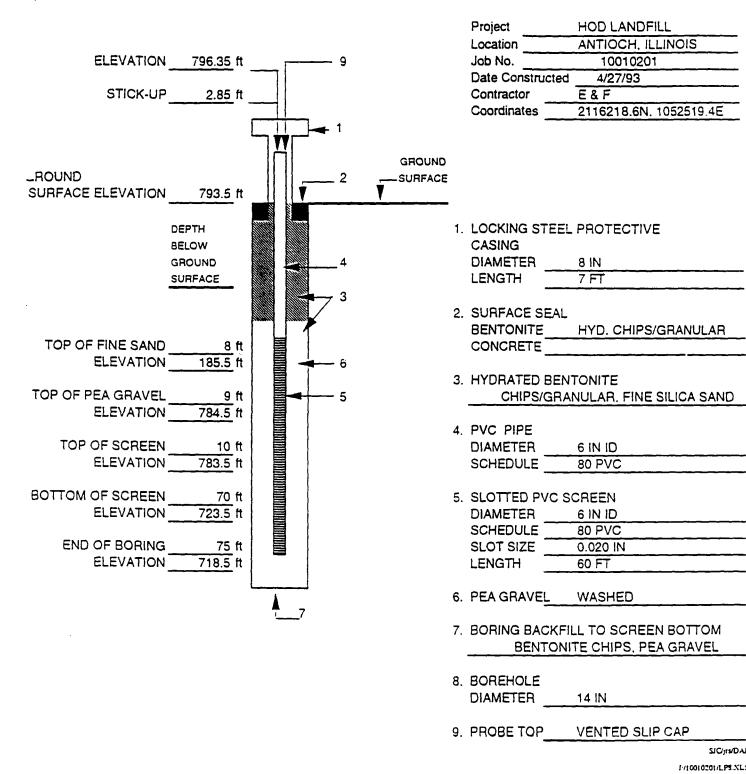




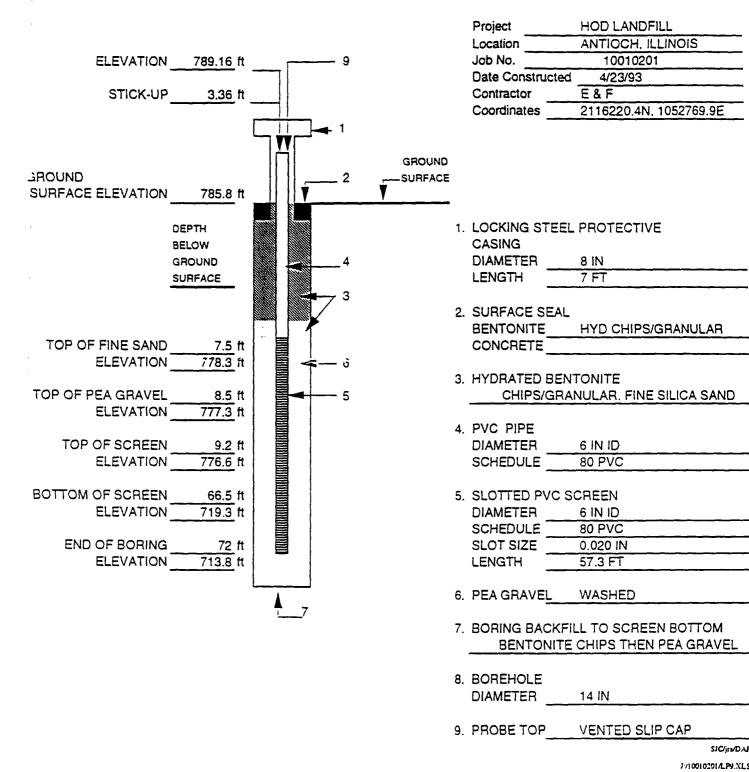
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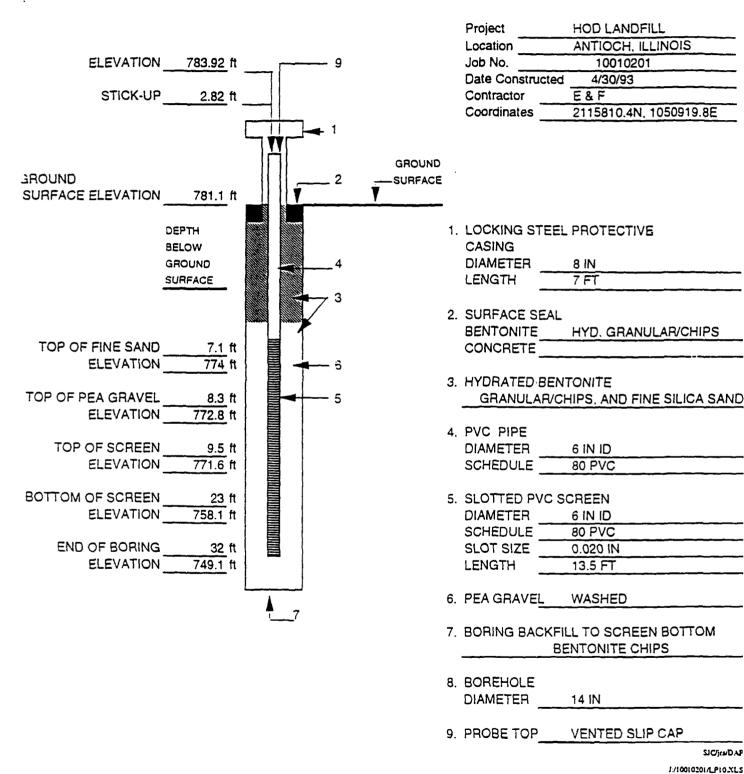




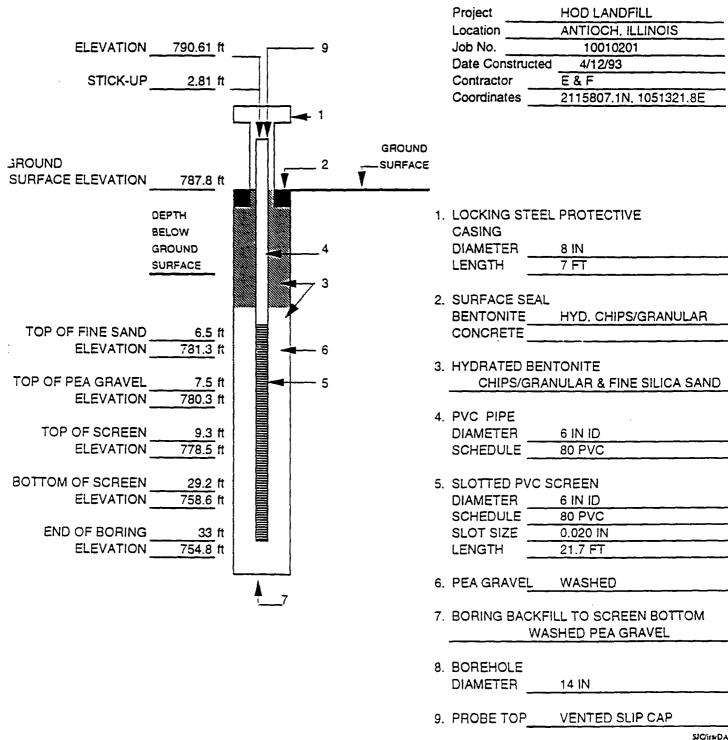






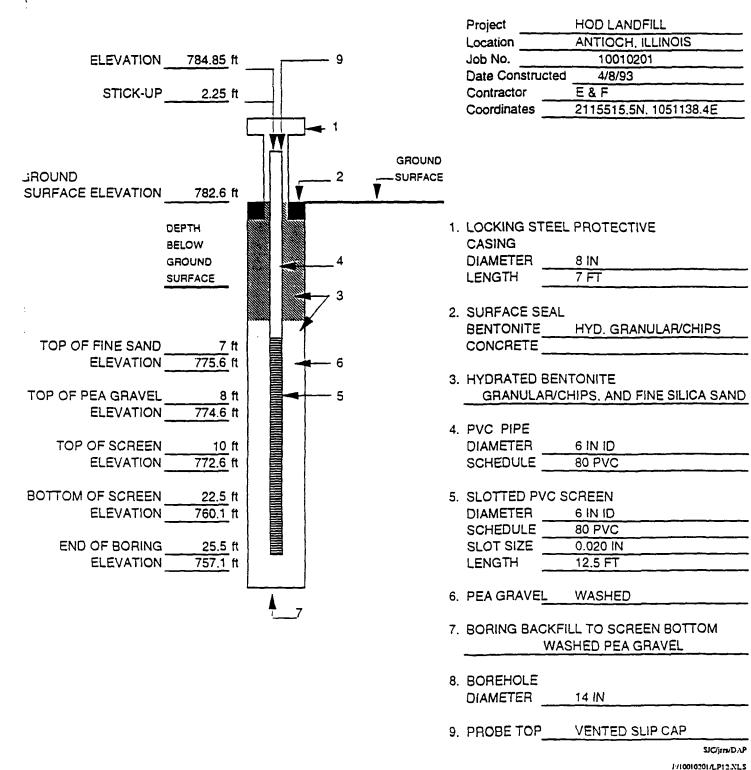




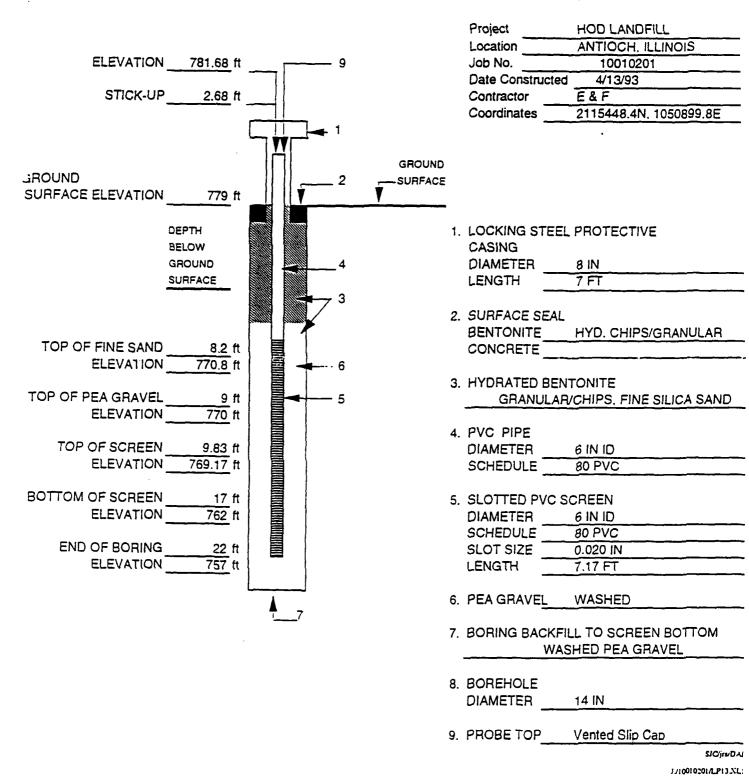


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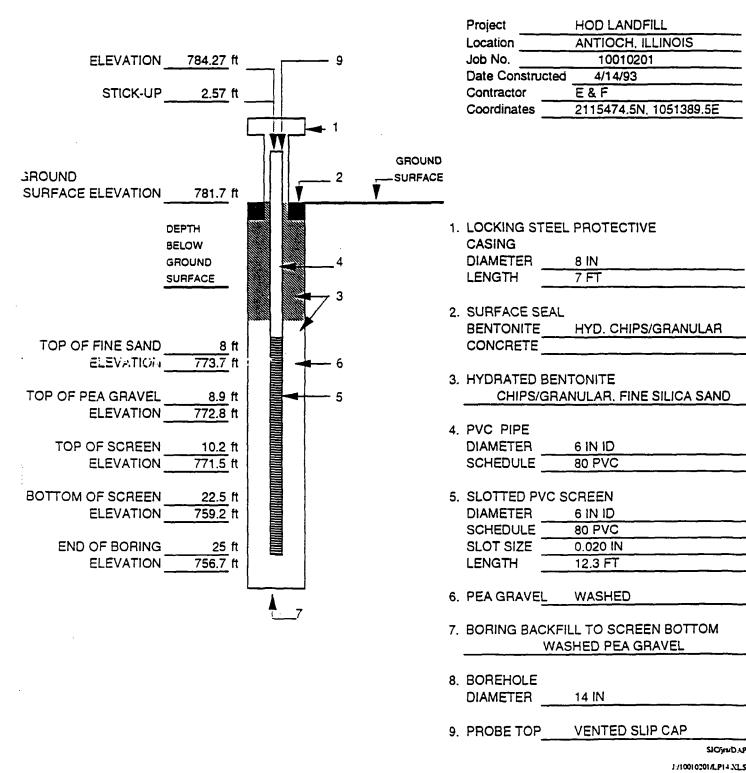




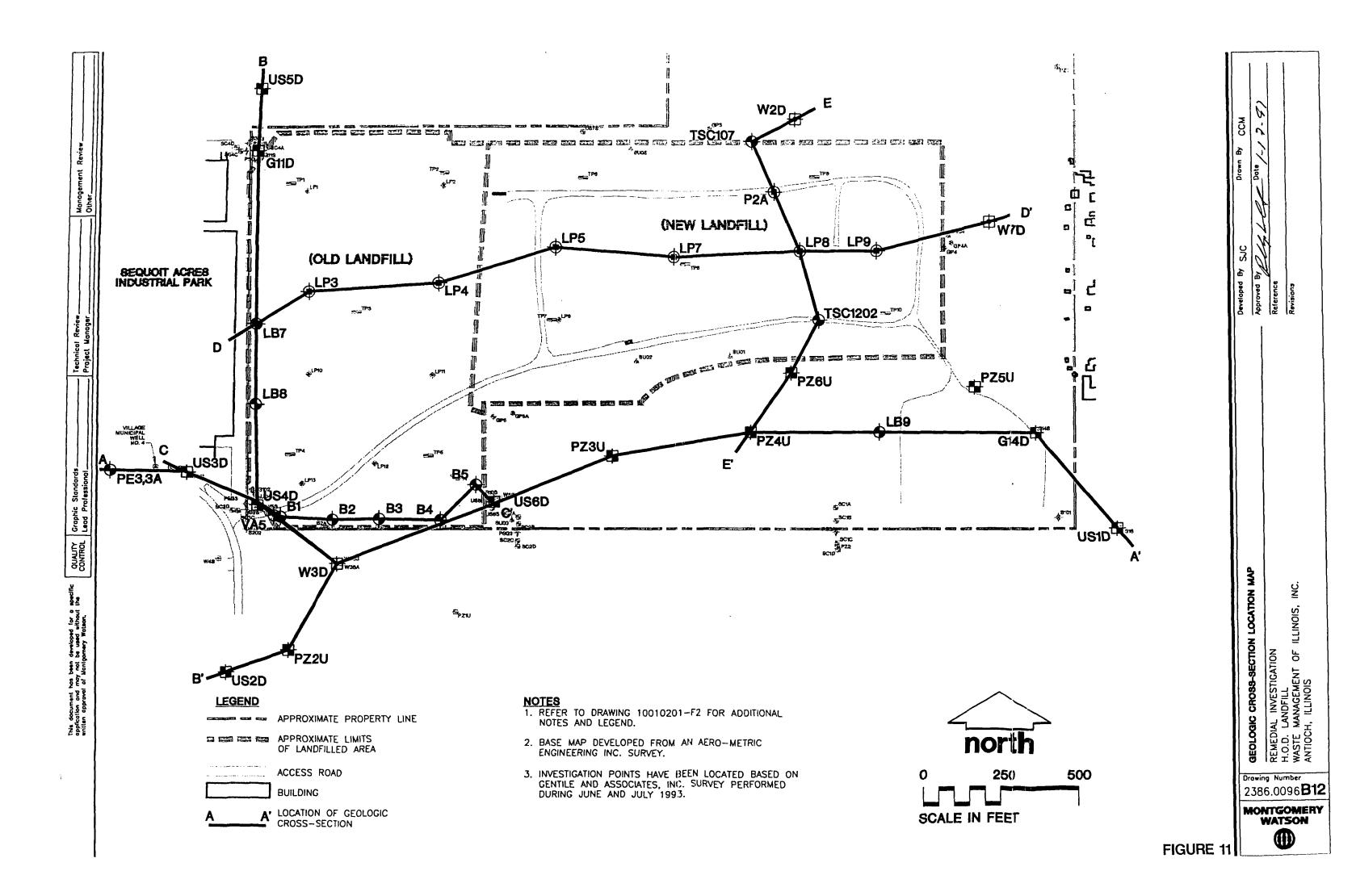




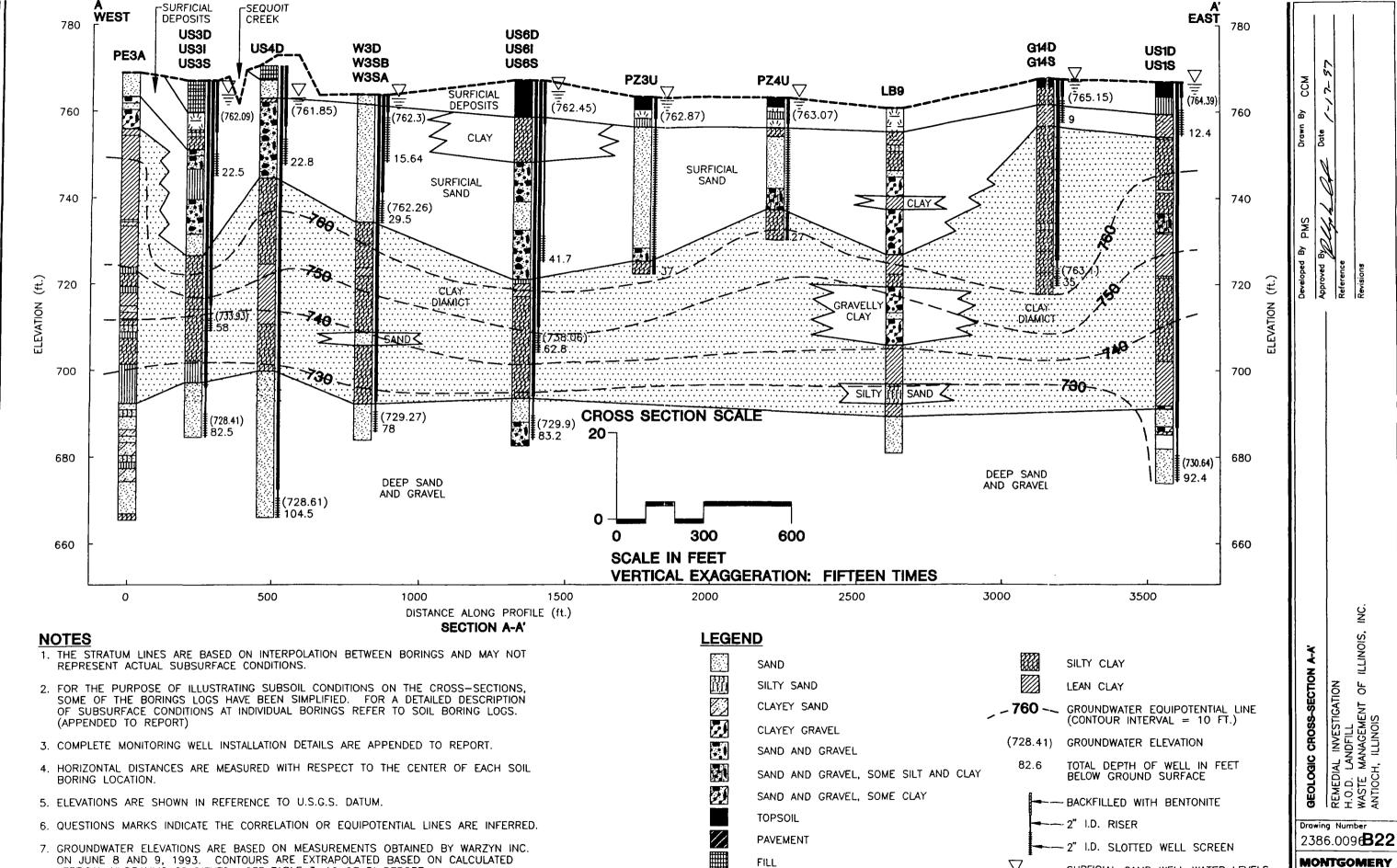




# Appendix D Geologic Cross Section



VERTICAL HYDRAULIC GRADIENTS. SEE TABLE 3-16 OF RI REPORT.



**REFUSE** 

SILT

SURFICIAL SAND WELL WATER LEVELS

FIGURE 12

WATSON

#### Appendix E Static Leachate Volume

PROJECT / PROPOSAL NAME / LOCATION: HO.D. LANDFIL	L. REMEDIAL DESIGN	PROJECT / PROPOSAL NO.
SUBJECT: LEACHATE VOLUME CALCULA	2	5314.08
PREPARED BY: JAMES TINSUM	DATE: 2/22/2000	FINAL O
CHECKED BY: (1) # 7 2/22/2000	DATE: 2/22/00	REVISION 🗇

#### OBJECTIVE

ESTIMATE THE CURRENT VOLUME OF EXTRACTABLE LEACHATE IN HO.D. LANDFILL BASED ON LEACHATE LEVELS MEASURED DURING THE NOVEMBER, 1999, ENGINEERING PREDECION INVESTIGATION AND A LEACHATE MAINTENANCE LEVEL OF EL 761.

#### BACKGROUND

AS PART OF THE USEPA APPROVED WORKPLAN FOR THE REMEDIAL DESIGN AT THE H.D.D. LANDFILL SITE, AN ESTIMATE OF THE VOLUME OF EXTRACTABLE LEACHATE WAS TO BE PREPARED. THIS COLCULATION SET IS INTENDED TO SATISFY THIS REQUIREMENT.

#### APPROACH

- 1) USE LERCHATE LEVELS OBTAINED DURING THE NOVEMBER OB AND DA, 1999, ENGINEERING PREDESIGN INVESTIGATION (PDI) AS THE TOP SURFACE FOR A VOLUME CALCULATION.
- 2) USE A LEACHATE MAINTENANCE ELEVATION OF 761 AS THE BASE SURFACE FOR A VOLUME CALCULATION.
- 3) PREPARE A TRIANGULATED VOLUME REPORT OVER THE LANDFILL FOOTPRINT.
- 4) ESTIMATE THE SPECIFIC YIELD OF THE LANDFILL MATERIAL.
- 5) CALCULATE VOLUME OF EXTRACTABLE LEACHATE BASED ON THE TRIANGULATED VOLUME (STEP 3) AND THE REPRESENTATIVE SPECIFIC YIELD (STEP 4).

#### ASSUMPTIONS

- 1) THE RATIO OF WASTE TO DAILY COVER AT THE SITE IS 6:1 (BASE) ON INDUSTRY STANDARD, RMT'S EXPERIENCE).
- 2) CALCULATION IS FOR STATIC CONDITION ONLY (I.E., NO INFLOW) OUTFLOW OF LEACHATE).
- 3) ESTIMATED SPECIFIC YIELD: FOR THE WASTE, USE A SPECIFIC YIELD OF 10% (OWE'S ET. AL, 1990) AS A REASONABLE VALUE FOR THE SHORT-TERM. IT IS IMPORTANT TO NOTE THAT AN EXACT ESTIMATE OF RECOVERABLE LEACHATE VOLUME IS DIFFICULT TO

PROJECT / PROPOSAL NAME / LOCATION: H.O.D. LANDI	TILL RD	PROJECT / PROPOSAL NO.
SUBJECT: LEACHATE VOLUME CALC	ULATION	5314.08
PREPARED BY: JAMES TINSUM	DATE: 2/22/2000	FINAL O
CHECKED BY: AH! MET	DATE: 2/22/00	REVISION 🗆

TO CALCULATE. THE YIELD IS A FUNCTION OF COMPACTION, AGE,
TEMPERATURE, COMPOSITION, AND SATURATION OF THE
WASTE AS WELL AS LANDFILL GAS CONTENT. AT H.O.D.
LANDFILL, THE WASTE IS A MINIMUM OF IS YEARS OLD, A
PORTION OF THE WASTE WAS BURNED AND A SIGNIFICANT
AMOUNT OF CONSOLIDATION HAS ALREADY OCCURRED. BASED ON
THESE CONDITIONS, A LOW SPECIFIC YIELD IS EXPECTED.

- 4) DAILY COVER DOES NOT CONTAIN RECOVERABLE LIQUID.
- 3) PERCHED LIOUD IS NOT IMMEDIATELY RECOVERABLE.

#### 212YJANA

MASS AT H.O.D. LANDFILL TO BE:

VOLUMETOTAL SAT, MASS = 940,431 CY

2) ACCOUNT FOR WASTE/COVER RATIO

$$V_{WASTE} = 940,431$$
 CY ×  $\frac{27CF}{CY}$  ×  $\frac{6}{7} = 21,764,260$  CF

$$V_{COVER} = 940,431 \text{ CY} \times \frac{27 \text{ CF}}{\text{CY}} \times \frac{1}{7} = 3,627,377 \text{ CF}$$

3) CALCULATE VOLUME OF EXTRACTABLE LEACHATE

VEXTRACTABLE LEAGUATE VWASTE MASS YIELD = 21,764,260 CF + 0.10 = 2,176,426 CF

4) CONVERT TO GALLONS

#### CONCLUSIONS

- 1) AN EXTRACTABLE VOLUME OF 16.3 MG OF LEACHATE IS REQUIRED TO LOWER LEACHATE LEVELS TO A MAINTENANCE ELEVATION OF 761.
- 2) TO MAINTAIN THIS LEVEL, CONTINUED EXTRACTION WOULD BE REQUIRED TO ACCOUNT FOR INFILTRATION, INFLOW FROM SURROUNDING AQUIFER, RECOVERY OF PERCHED LEACHATE, AND CONTINUED WASTE CONSOLIDATION.

PROJECT / PROPOSAL NAME / LOCATION: 4.0.D. LAI	VDFILL, RD	PROJECT / PROPOSAL NO.
SUBJECT: LEACHATE VOLUME CALC	ULATION	53/4.08
PREPARED BY: JAMES TINJUM	DATE: 2/22/2000	FINAL 🗇
CHECKED BY: ( M. I.T.	DATE: 2/22/00	REVISION 🗆

#### REFERENCES

OWEIS, 1.5. ET. AL (1990). HYDRAULIC CHARACTERISTICS OF MUNICIPAL REFUSE. J. OF GEOTECHNICAL ENGINEERING, VOL. 116 (4), APRIL, 1990.

RMT, INC. (2000), PREDECIGN INVESTIGATION RESULTS, LANDFILL GAS AND LEACHATE, FEBRUARY, 2000.

ATTACHMENT 1



#### **COMPUTATION SHEET**

							SHEET	Γ	1	_ OF	1
744 Heartland Trail (53717-8923)	P.O. Box	8923 (53708	3-8923)	Madisor	ı, WI	(608) 8	31-4444	FAX:	(608) 831-3334	VOICE:	(608) 831-1989
PROJECT/PROPOSAL NAME		PREPARI	ED.		CHE	CKED			PROJECT/PR	OPOSAL	NO.
H.O.D. LANDFILL	By: Dat		te: 10-00	1 '		Date: 1/26/	/00		5314.04		
					Mg	7	2/22/	100			

#### STATIC VOLUME OF LEACHATE

#### Purpose:

To determine the volume of saturated waste and soil between the top of leachate levels to an elevation of 761 MSL.

#### **Methodology:**

After the leachate grades and wellbase grades are developed, *Intergraph's design software* "Siteworks" was utilized to generate and compare a digital terrain models (3-dimensional surface model) of each. These two surfaces, leachate and wellbase, were compared by the triangle method using "Siteworks" to determine the site capacity (volume) within the limits of waste.

Design File: j:\05314\04\leachate.dgn

 $\underline{\textbf{Original Surface:}} \quad j: \ 05314 \ 04 \ dtm \ leachate. dtm$ 

Design Surface: j:\05314\04\dtm\wellbase.dtm

Calculations:

☐ Grid Volume: 'Interval☐ Selected Shapes: Level☒ Triangle Volume

Original Surface: measured leachate volume within the limits of waste

Design Surface: assumed bottom of wells @ elevation 761.0'

 Cut
 Fill
 Net

 (cu yd)
 (cu yd)
 (cu yd)

 949,258.14
 8,827.48
 940,430.65

#### **Results:**

Static volume of leachate is ~940,431 cu yd.